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Environmental Impact Management Services (Pty) Ltd

QUANTITATIVE RISK ASSESSMENT OF THE PROPOSED CCGT AT KELVIN POWER STATION, KEMPTON PARK

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QUANTITATIVE RISK ASSESSMENT OF THE PROPOSED CCGT AT KELVIN POWER STATION, KEMPTON PARK

EXECUTIVE SUMMARY

1 INTRODUCTION

Kelvin Power Pty Ltd (“Kelvin”) is a coal fired power plant situated in Kempton Park, Johannesburg, South Africa, owned by the Anergi group (“Anergi”) and Public Investment Corporation (“PIC”). The existing power plant comprises of: (i) the still operational B Station which was built in the 1960s and includes seven 60 MW steam turbines and eight pulverised coal boilers, and (ii) the now decommissioned A Station which was built in the 1950s. The A station ceased operations in 2012 and a Basic Assessment has been approved for its demolition.

A pre-feasibility study was concluded in 2023 to assess the various technology options available to generate 450 MW to 650 MW on the current A Station site. The pre-feasibility study’s objective was to identify proven technology available for generation on the available site considering the infrastructure available. The study concluded that a combined-cycle gas turbine (CCGT) Power Plant with a net output of approximately 600 MW comprising one H class gas turbine, a heat recovery boiler and a steam turbine, would be the optimum technology for this site. The plant is expected to operate as a mid-merit plant with an annual average capacity factor of 50%.

The main structures at the plant would consist of:

- Gas turbine building;
- Steam turbine building;
- Heat Recovery Steam Generator (HRSG);
- Mechanical draft cooling tower;
- Extra High Voltage (EHV) substation;
- Auxiliary buildings;
- Administration buildings; and,
- Exhaust stack.

The site allocated to the new plant is in the area of the redundant A Station auxiliary plant formerly occupied by the A Station dry coal store, coal tipplers, coal stockpile and cooling towers. In addition to the construction area of the permanent plant, other construction facilities such as laydown areas, fabrication shops, warehousing, construction offices, and welfare facilities would be required. The A Station auxiliary plant area is sufficient to accommodate both the permanent plant and the construction facilities outlined above.

Cooling water would be sourced from the existing Kelvin water supply pipelines. Treated sewage wastewater (grey water) would be supplied to the power plant from Diepsloot ~37 km away for use as cooling water. Approximately 52 033 m³ per day of such water has previously been supplied to the Kelvin power plant and as such, quantity would be available for the new plant. The new plant is expected to consume approximately 11 000 m³ per day of water per day when operating as a mid-merit plant with a capacity factor of 50%. The Diepsloot pump

house and water pipeline to the plant is the responsibility of, and is maintained by, Kelvin Power. The grey water is dosed with biocides, algaecides, and a corrosion inhibitor.

In addition to the new plant that would be constructed on the Kelvin site, an electrical connection to an Eskom / City Power substation and a gas pipeline to the Sasol gas pipeline system would be required. Should the new plant be connected to the City Power Sebenza substation, a transmission line of approximately 1 km would be required. Alternatively, if the connection was to the Eskom North Rand substation, a transmission line of approximately 5 km would be required. Construction of this transmission line would be the responsibility of Kelvin. A new 25 km gas supply pipeline connecting the new plant to the Sasol high pressure gas transmission system would be required. Construction of this gas supply pipeline would be the responsibility of Sasol.

Since off-site incidents may result due to hazards of some of the chemical components to be stored on, produced at or delivered to site, RISCOM (PTY) LTD was commissioned to conduct a quantitative risk assessment (QRA), the impacts onto surrounding properties and communities as part of an environmental impact assessment (EIA).

1.1 Terms of Reference

The main aim of the investigation was to quantify the risks to employees, neighbours and the public with regard to the proposed CCGT facility at Kempton Park.

This risk assessment was conducted in accordance with the MHI regulations and can be used as notification for the facility. The scope of the risk assessment included:

Development of accidental spill and fire scenarios for the facility;
Using generic failure rate data (for tanks, pumps, valves, flanges, pipework, gantry, couplings and so forth), determination of the probability of each accident scenario;
For each incident developed in Step 2, determination of consequences (such as thermal radiation, domino effects, toxic-cloud formation and so forth);

1. For scenarios with off-site consequences (greater than 1% fatality off-site), calculation of maximum individual risk (MIR), taking into account all generic failure rates, initiating events (such as ignition), meteorological conditions and lethality.

1.2 Purpose and Main Activities

The main activity of the proposed CCGT would be the generation of mid-merit power supply to the South African electricity grid. The fuel used to generate power would be natural gas, that will be delivered to site by pipeline.

1.3 Main Hazards Due to Substance and Process

The main hazards that would occur with a loss of containment of hazardous components at the proposed CCGT facility in Kempton Park include exposure to:

- Thermal radiation from fires;
- Toxic gas releases; and
- Overpressure from explosions.

2 ENVIRONMENT

The site location for the proposed CCGT facility is at the current Kelvin Power Station, as shown in Figure 2-1.

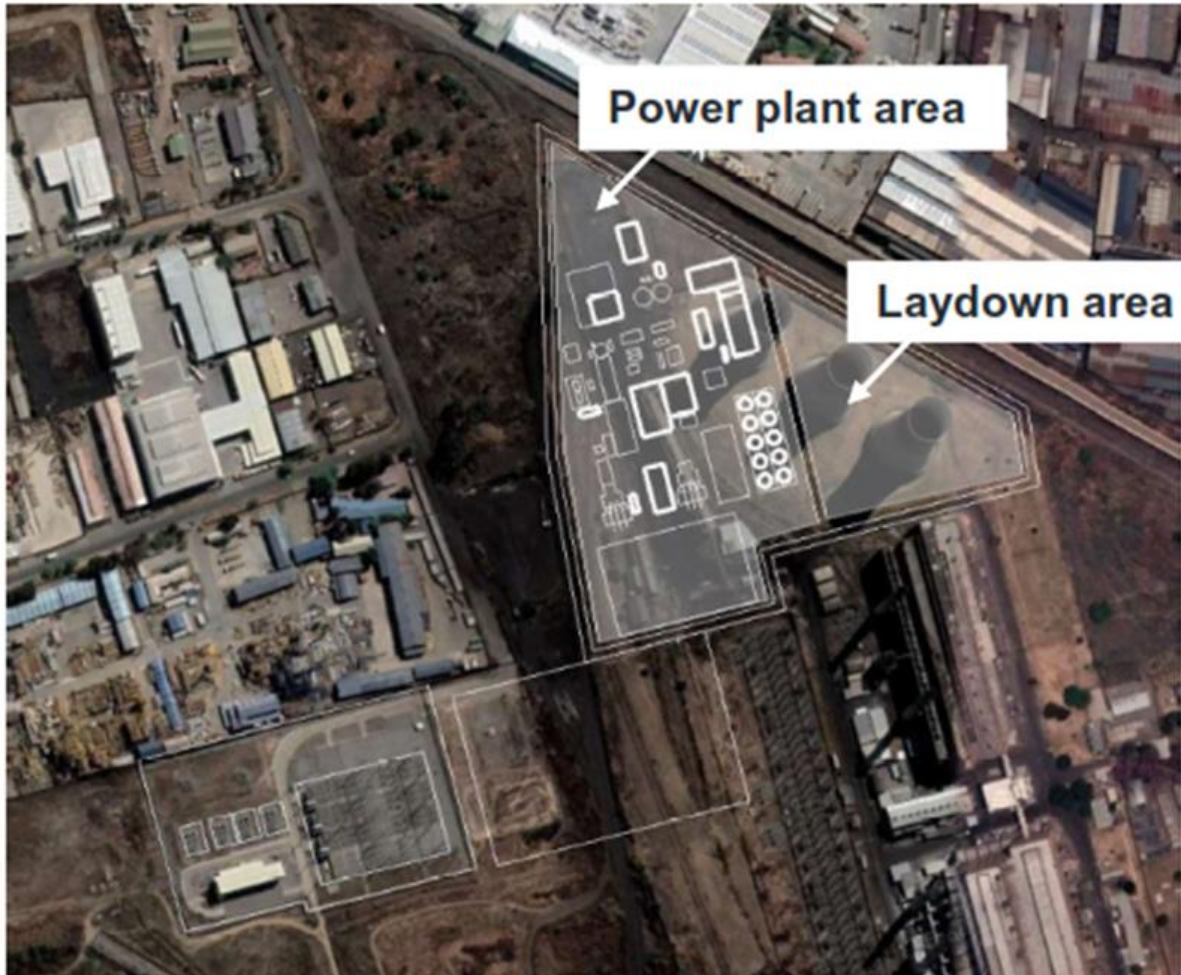


Figure 2-1: Proposed CCGT location at the Kelvin Power Station

The Kelvin Power Station has an access control point, whereby all traffic and people are controlled. Thus, all people entering the site will be limited to workers, and the general public will not have access to free movement within the zoned area.

The land use surrounding the proposed CCGT facility is shown in Figure 2-1.

The Kelvin Power Station is located between the suburbs of Kempton Park and Edenvale. The closest residential area is Cresslawn approximately 300 m east of the proposed CCGT facility.

3 PROCESS DESCRIPTION

3.1 Site

The proposed CCGT facility in Kempton Park is to consist offices, workshops, gas and steam turbines and associated equipment, as shown in Figure 3-1.

The site will be accessed via the main entrance of Kelvin. Thus, all unauthorised people and the general public will be excluded from the power station.

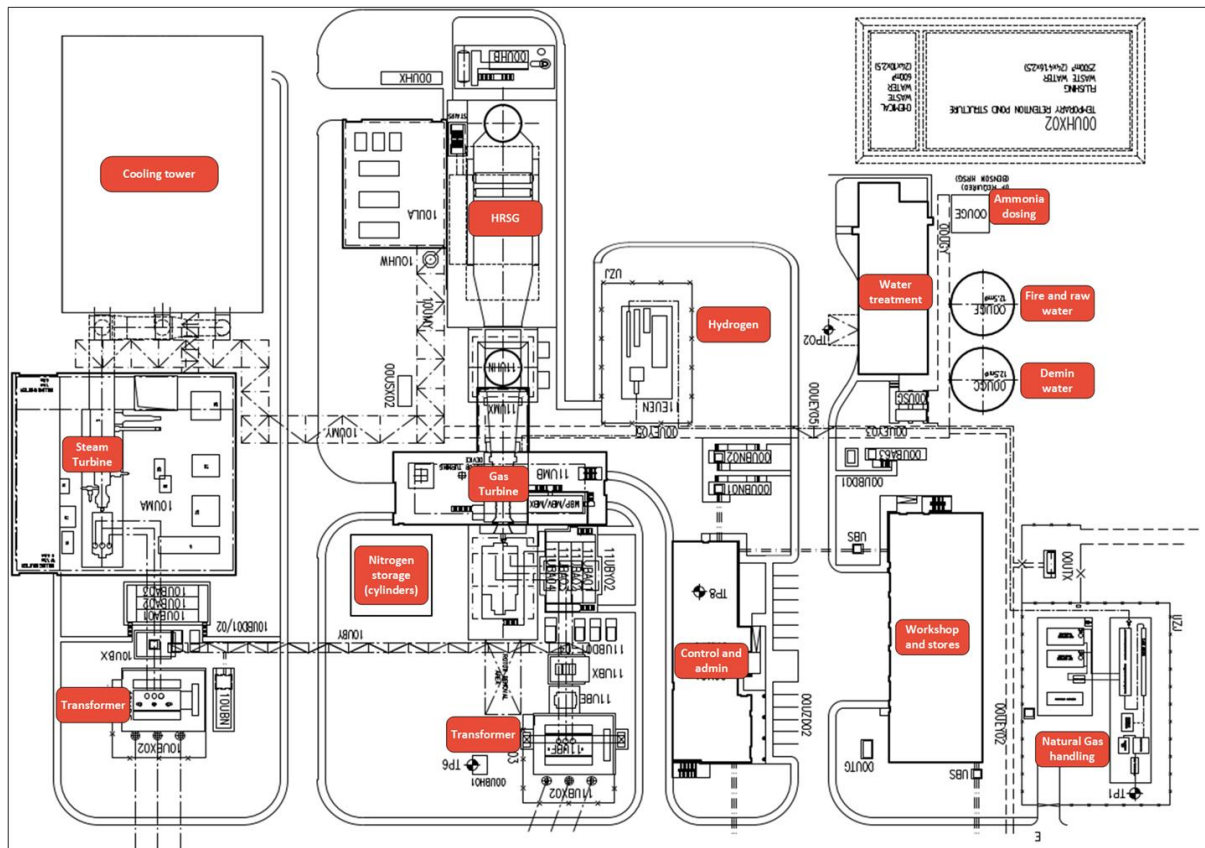


Figure 3-1: Site layout

3.2 Process Description

The project will consist of up to 3 CCGTs used to produce a nominal capacity of 600 MW power from natural gas (in either liquid or gas forms) or a mixture of natural gas and hydrogen (in a proportion scaling up from 30% hydrogen - H₂) as a fuel.

The process for converting the energy in a fuel into the electric power involves the creation of mechanical work, which is then transformed into the electric power by a generator. The overall efficiency of the conversion depending on the type of fuel and the thermodynamics process used and it can be as low as 30%.

To increase the overall efficiency of electric power plants, multiple thermodynamic processes can be introduced or combined to recover and utilize the residual heat energy in hot exhaust gases. By the use of combined cycle, power plants can achieve the electrical efficiency up to 60%.

The terms “combined cycle” refers to the combining of multiple thermodynamic cycles to generate electric power. Combined cycle operation uses a heat recovery steam generator (HRSG) that captures the heat from high temperature exhaust gases to produce steam, which is then supplied to a steam turbine to generate additional electric power. The process for creating steam to produce work using a steam turbine is based on the Rankine cycle.

The most common type of combined cycle power plant utilizes gas turbines and is called a combined cycle gas turbine (CCGT) plant. Because gas turbines have low efficiency in simple cycle operation and the output produced by the steam turbine accounts for about half of the CCGT plant output.

The simplified schematic of the CCGT power plant is shown in Figure 3-2.

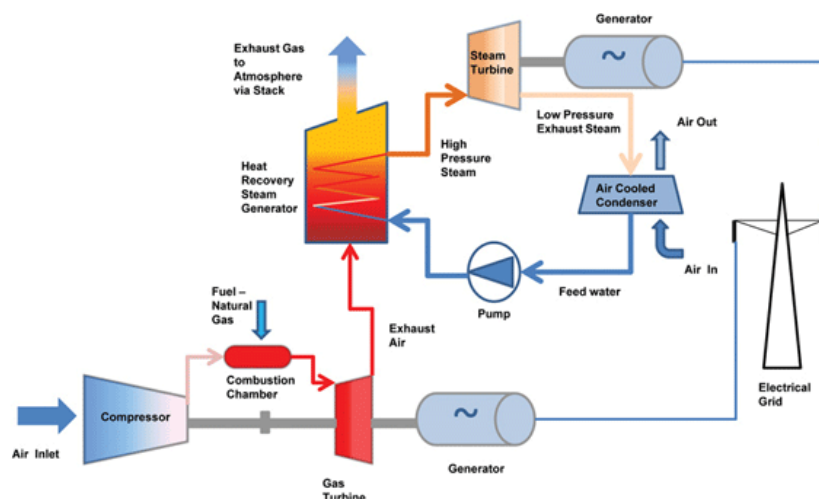


Figure 3-2: Simplified schematic of a CCGT power plant

3.3 Fuel and Process Chemicals

3.3.1 Natural Gas

Natural gas would be used to fuel the gas turbines. The gas will be supplied via a pipeline. This study assumes a gas supply pressure of 46 bar. No storage of natural gas would be provided.

3.3.2 Diesel

A 24 m³ diesel storage tank would be provided for emergency power.

3.3.3 Hydrogen

One hydrogen trailer has been provided in the design. The trailer is assured to be that of a standard hydrogen trailer of 190 kg hydrogen inventory with a storage pressure at 226 bar(g).

3.3.4 Ammonia

Ammonia would be used to adjust the pH of the boiler water feed. The size and storage details of the ammonia has not been provided. However, a 10 m³ ammonia tank was assumed.

3.3.5 Nitrogen

Nitrogen would be required to purge natural gas in pipelines and equipment prior to conducting maintenance.

The nitrogen designs have not been specified at this stage of the project.

4 METHODOLOGY

The first step in any risk assessment is to identify all hazards. The merit of including a hazard for further investigation is then determined by how significant it is, normally by using a cut-off or threshold value.

Once a hazard has been identified, it is necessary to assess it in terms of the risk it presents to the employees and the neighbouring community. In principle, both probability and consequence should be considered, but there are occasions where, if either the probability or the consequence can be shown to be sufficiently low or sufficiently high, decisions can be made based on just one factor.

During the hazard identification component of the report, the following considerations are taken into account:

- Chemical identities;
- Location of on-site installations that use, produce, process, transport or store hazardous components;
- Type and design of containers, vessels or pipelines;
- Quantity of material that could be involved in an airborne release;
- Nature of the hazard most likely to accompany hazardous materials spills or releases, e.g., airborne toxic vapours or mists, fires or explosions, large quantities to be stored and certain handling conditions of processed components.

The evaluation methodology assumes that the facility will perform as designed in the absence of unintended events such as component and material failures of equipment, human errors, external events and process unknowns.

SANS 1461 (2018) is based on RIVM (2009) for process plants. The latter standards describe the minimum scenarios to be included in the assessment, as well as the assumptions to be used. As full compliance of SANS 1461 (2018) cannot be achieved within the NEMA legislative framework, general compliance of the aforementioned standards at this stage would be applicable and briefly described in the sections below. This general compliance assessment constitutes a quantitative risk assessment (QRA).

The QRA process is summarised with the following steps:

1. Identification of components that are flammable, toxic, reactive or corrosive and that have potential to result in a major incident from fires, explosions or toxic releases;
2. Development of accidental loss of containment (LOC) scenarios for equipment containing hazardous components (including release rate, location and orientation of release);
3. For each incident developed in Step 2, determination of consequences (such as thermal radiation, domino effects, toxic-cloud formation and so forth);
4. For scenarios with off-site consequences (greater than 1% fatality off-site), calculation of maximum individual risk (MIR), taking into account all generic failure rates, initiating events (such as ignition), meteorological conditions and lethality.

5 CONCLUSIONS

Risk calculations are not precise. Accuracy of predictions is determined by the quality of base data and expert judgements.

This risk assessment included the consequences of fires and explosions at the proposed CCGT facility in Kempton Park. A number of well-known sources of incident data were consulted and applied to determine the likelihood of an incident to occur.

This risk assessment was performed with the assumption that the site would be maintained to an acceptable level and that all statutory regulations would be applied. It was also assumed that the detailed engineering designs would be done by competent people, and would be correctly specified for the intended duty. For example, it was assumed that tank wall thicknesses have been correctly calculated, that vents have been sized for emergency conditions, that instrumentation and electrical components comply with the specified electrical area classification, that material of construction is compatible with the products, etc.

It is the responsibility of the owners and their contractors to ensure that all engineering designs would have been completed by competent persons, and that all pieces of equipment would have been installed correctly. All designs should be in full compliance with (but not limited to) the Occupational Health and Safety Act 85 of 1993 and its regulations, the National Buildings Regulations and the Buildings Standards Act 107 of 1977 as well as local bylaws.

A number of incident scenarios were simulated, taking into account the prevailing meteorological conditions, and described in the report.

5.1 Notifiable Substances

The General Machinery Regulation 8 and its Schedule A on notifiable substances, requires any employer who has a substance equal to or exceeding the quantity listed in the regulation to notify the divisional director. A site is classified as a Major Hazard Installation if it contains one or more notifiable substances, or if the off-site risk is sufficiently high. The latter can only be determined from a quantitative risk assessment.

The notifiable threshold for ammonia is listed as 20 tonne in a single vessel. As the proposed installation should not exceed the threshold limit, ammonia will not be classified as a notifiable substance.

5.2 Power Plant and Associated Equipment

Hazardous substances associated with this facility would include; ammonia; hydrogen, diesel and natural gas. Of the listed substances, only ammonia and natural gas could result in offsite fatalities.

The risk of 1×10^{-6} fatalities per person per year isopleth found to be immediately beyond but primarily within the site boundary.

5.3 Impacts onto Neighbouring Properties, Residential Areas and MHIs

A large release of ammonia could extend a considerable downward distance impacting the commercial and residential areas of Kempton Park, Edenvale and Lethabong. However, fatalities will be limited to the industrial area and will not impact residential areas.

No residential area or vulnerable institutions would be seriously impacted with the construction and operation of the proposed CCGT.

5.4 Major Hazard Installation

This investigation concluded that under the current design conditions, the proposed CCGT facility in Kempton Park **would be considered as a Major Hazard Installation** and would require notification in accordance with the MHI regulations.

According to chapter 3 the “Classification of pipelines as major hazard establishment” of Major Hazard Installation Regulations, 2022:

A pipeline is considered an establishment if it contains a fluid which is or is to be conveyed in a pipeline as a gas which is flammable in air (is applicable to flammable gases conveyed as a gas. In such cases the additional duties only apply when the flammable gas is conveyed at a pressure in excess of 8 bars absolute. This covers such fluids as methane, butane and propane).

Kindly note that this study is not intended to replace the Major Hazard Installation risk assessment, which should be completed prior to construction of the terminal once final designs are available.

6 RECOMMENDATIONS

As a result of the risk assessment study conducted for the proposed CCGT facility in Kempton Park, a number of events were found to have risks beyond the site boundary. These risks could be mitigated to acceptable levels, as shown in the report.

RISCOM did not find any fatal flaws that would prevent the project proceeding to the detailed engineering phase of the project, and would support the project under the following conditions most of which will be detailed in the MHI study:

- Compliance with all statutory requirements, i.e., pressure vessel designs;
- Compliance with applicable SANS codes, i.e., SANS 10087, SANS 10089, SANS 10108, etc. ;
- Incorporation of applicable guidelines or equivalent international recognised codes of good design and practice into the designs;
- Completion of a recognised process hazard analysis (such as a HAZOP study, FMEA, etc.) on the proposed facility prior to construction to ensure design and operational hazards have been identified and adequate mitigation put in place;
- Full compliance with IEC 61508 and IEC 61511 (Safety Instrument Systems) standards or equivalent to ensure that adequate protective instrumentation is included in the design and would remain valid for the full life cycle of the tank farm:
 - Including demonstration from the designer that sufficient and reliable instrumentation would be specified and installed at the facility;
- Preparation and issue of a safety document detailing safety and design features reducing the impacts from fires, explosions and flammable atmospheres to the MHI assessment body at the time of the MHI assessment:
 - Including compliance to statutory laws, applicable codes and standards and world's best practice;
 - Including the listing of statutory and non-statutory inspections, giving frequency of inspections;
 - Including the auditing of the built facility against the safety document;
 - Noting that codes such as IEC 61511 can be used to achieve these requirements;
- Demonstration by the CCGT owner or their contractor that the final designs would reduce the risks posed by the installation to the South African requirements as prescribed in SANS 1461 (2018);
- Signature of all terminal designs by a professional engineer registered in South Africa in accordance with the Professional Engineers Act, who takes responsibility for suitable designs;
- Completion of an emergency preparedness and response document for on-site and off-site scenarios prior to initiating the MHI risk assessment (with input from local authorities);
- Any increases to the product list or product inventories must be with the approval of the authorities under NEMA;
- Final acceptance of the facility risks with an MHI risk assessment that must be completed in accordance with the MHI regulations;
 - Basing such a risk assessment on the final design and including engineering mitigation.

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QUANTITATIVE RISK ASSESSMENT OF THE PROPOSED CCGT AT KELVIN POWER STATION, KEMPTON PARK

1 INTRODUCTION

Kelvin Power Pty Ltd (“Kelvin”) is a coal fired power plant situated in Kempton Park, Johannesburg, South Africa, owned by the Anergis group (“Anergis”) and Public Investment Corporation (“PIC”). The existing power plant comprises of: (i) the still operational B Station which was built in the 1960s and includes seven 60 MW steam turbines and eight pulverised coal boilers, and (ii) the now decommissioned A Station which was built in the 1950s. The A station ceased operations in 2012 and a Basic Assessment has been approved for its demolition.

A pre-feasibility study was concluded in 2023 to assess the various technology options available to generate 450 MW to 650 MW on the current A Station site. The pre-feasibility study’s objective was to identify proven technology available for generation on the available site considering the infrastructure available. The study concluded that a combined-cycle gas turbine (CCGT) Power Plant with a net output of approximately 600 MW comprising one H class gas turbine, a heat recovery boiler and a steam turbine, would be the optimum technology for this site. The plant is expected to operate as a mid-merit plant with an annual average capacity factor of 50%.

The main structures at the plant would consist of:

- Gas turbine building;
- Steam turbine building;
- Heat Recovery Steam Generator (HRSG);
- Mechanical draft cooling tower;
- Extra High Voltage (EHV) substation;
- Auxiliary buildings;
- Administration buildings; and,
- Exhaust stack.

The site allocated to the new plant is in the area of the redundant A Station auxiliary plant formerly occupied by the A Station dry coal store, coal tipplers, coal stockpile and cooling towers. In addition to the construction area of the permanent plant, other construction facilities such as laydown areas, fabrication shops, warehousing, construction offices, and welfare facilities would be required. The A Station auxiliary plant area is sufficient to accommodate both the permanent plant and the construction facilities outlined above.

Cooling water would be sourced from the existing Kelvin water supply pipelines. Treated sewage wastewater (grey water) would be supplied to the power plant from Diepsloot ~37 km away for use as cooling water. Approximately 52 033 m³ per day of such water has previously been supplied to the Kelvin power plant and as such, quantity would be available for the new plant. The new plant is expected to consume approximately 11 000 m³ per day of water per day when operating as a mid-merit plant with a capacity factor of 50%. The Diepsloot pump house and water pipeline to the plant is the responsibility of, and is maintained by, Kelvin Power. The grey water is dosed with biocides, algacides, and a corrosion inhibitor.

In addition to the new plant that would be constructed on the Kelvin site, an electrical connection to an Eskom / City Power substation and a gas pipeline to the Sasol gas pipeline system would be required. Should the new plant be connected to the City Power Sebenza substation, a transmission line of approximately 1 km would be required. Alternatively, if the connection was to the Eskom North Rand substation, a transmission line of approximately 5 km would be required. Construction of this transmission line would be the responsibility of Kelvin. A new 25 km gas supply pipeline connecting the new plant to the Sasol high pressure gas transmission system would be required. Construction of this gas supply pipeline would be the responsibility of Sasol.

Since off-site incidents may result due to hazards of some of the chemical components to be stored on, produced at or delivered to site, RISCUM (PTY) LTD was commissioned to conduct a quantitative risk assessment (QRA), the impacts onto surrounding properties and communities as part of an environmental impact assessment (EIA).

1.1 Legislation

Legislation discussed in this subsection is limited to the health and safety of employees and the public.

Risk assessments are conducted when required to do so by law, or by companies wishing to determine the risks of the facility for other reasons, such as insurance.

In South Africa, risk assessments are carried out under the legislation of two separate acts, each with different requirements. These are discussed in the subsections that follow.

1.1.1 National Environmental Management Act (No. 107 of 1998) (NEMA) and its Regulations

The National Environmental Management Act (NEMA) contains South Africa's principal environmental legislation. It has, as its primary objective to make provision for cooperative governance by establishing principles for decision making on matters affecting the environment, on the formation of institutions that will promote cooperative governance and on establishing procedures for coordinating environmental functions exercised by organs of state, as well as to provide for matters connected therewith (Government Gazette 1998).

Section 30 of the NEMA act deals with the control of emergency incidents where an "incident" is defined as an *"unexpected sudden occurrence, including a major emission, fire or explosion leading to serious danger to the public or potentially serious pollution of or detriment to the environment, whether immediate or delayed"*.

The act defines "pollution" as *"any change in the environment caused by:*

- (i) Substances;
- (ii) Radioactive or other waves; or,
- (iii) Noise, odours, dust or heat...

" Emitted from any activity, including the storage or treatment of waste or substances, construction and the provision of services, whether engaged in by any person or an organ of state, where that change has an adverse effect on human health or wellbeing or on the composition, resilience and productivity of natural or managed ecosystems, or on materials useful to people, or will have such an effect in the future..."

“Serious” is not fully defined but would be accepted as having long lasting effects that could pose a risk to the environment, or to the health of the public that is not immediately reversible.

This is similar to the definition of a Major Hazard Installation (MHI) as defined in the Occupational Health and Safety Act (OHS Act) 85 of 1993 and its MHI regulations.

Section 28 of NEMA makes provision for anyone who causes pollution or degradation of the environment being made responsible for the prevention of the occurrence, continuation or reoccurrence of related impacts and for the costs of repair of the environment. In terms of the provisions under Section 28 that are stated as:

“ *Every person who causes, has caused or may cause significant pollution or degradation of the environment must take reasonable measures to prevent such pollution or degradation from occurring, continuing or recurring, or, in so far as such harm to the environment is authorised by law or cannot reasonably be avoided or stopped...* ”

1.1.2 The Occupational Health and Safety Act No. 85 of 1993

The Occupational Health and Safety Act 85 (1993) is primarily intended for the health and safety of the employees, whereas its MHI regulations is intended for the health and safety of the public.

The OHS Act shall not apply in respect of:

- “
- a) *A mine, a mining area or any works as defined in the Minerals Act, 1991 (Act No. 50 of 1991), except in so far as that Act provides otherwise;*
 - b) *Any load line ship (including a ship holding a load line exemption certificate), fishing boat, sealing boat and whaling boat as defined in Section 2 (1) of the Merchant Shipping Act, 1951 (Act No. 57 of 1951), or any floating crane, whether or not such ship, boat or crane is in or out of the water within any harbour in the Republic or within the territorial waters thereof, (date of commencement of paragraph (b) to be proclaimed.), or in respect of any person present on or in any such mine, mining area, works, ship, boat or crane.* ”

1.1.2.1 Major Hazard Installation Regulations

The MHI regulations (July 2001) published under Section 43 of the OHS Act require employers, self-employed persons and users who have on their premises, either permanently or temporarily, a major hazard installation or a quantity of a substance which may pose a **risk** (our emphasis) that could affect the health and safety of employees and the public to conduct a risk assessment in accordance with the legislation.

On the 31st of January 2023, new MHI regulations were gazetted, whereby the facility would be classified based on the quantity of hazardous products stored on site. The threshold values for these hazardous products are defined within the Regulations.

In accordance with legislation, the risk assessment must be done by an approved inspection authority (AIA), which is registered with the Department of Employment and Labour and accredited by the South African Accreditation Systems (SANAS). Furthermore, the

Engineering Professional Act 114 of 2000, requires all persons conducting engineering work to be registered with the Engineering Council of South Africa and may not perform work outside of their field of registration. Copies of the relevant certificates are given in Appendix C and Appendix D.

Similar to Section 30 of NEMA as it relates to the health and safety of the public, the MHI regulations are applicable to the health and safety of employees and the public in relation to the operation of a facility, and specifically in relation to sudden or accidental major incidents involving substances that could pose a risk to the health and safety of employees and the public.

The notification of the MHI is described in the regulations as an advertisement placement and specifies the timing of responses from the advertisement. It should be noted that the regulation does not require public participation.

The regulations, summarised in Appendix A, essentially consists of various parts, namely:

1. The duties for notification and registration of a MHI;
2. The minimum requirements for a QRA;
3. Major incident prevention policy;
4. Safety report;
5. Licence to operate;
6. The general duties required of local government;
7. The requirements for an on-site emergency plan;
8. The reporting steps for risk and emergency occurrences;
9. Information and training;
10. The general duties required of suppliers;
11. The duties of approved inspection authority.

As this is not an MHI risk assessment, the application of the above legislation is not mandatory but the legislation is described to give a background to this report.

1.2 Terms of Reference

The main aim of the investigation was to quantify the risks to employees, neighbours and the public with regard to the proposed CCGT facility at Kempton Park.

This risk assessment was conducted in accordance with the MHI regulations and can be used as notification for the facility. The scope of the risk assessment included:

1. Development of accidental spill and fire scenarios for the facility;
2. Using generic failure rate data (for tanks, pumps, valves, flanges, pipework, gantry, couplings and so forth), determination of the probability of each accident scenario;
3. For each incident developed in Step 2, determination of consequences (such as thermal radiation, domino effects, toxic-cloud formation and so forth);
4. For scenarios with off-site consequences (greater than 1% fatality off-site), calculation of maximum individual risk (MIR), taking into account all generic failure rates, initiating events (such as ignition), meteorological conditions and lethality.

1.3 Purpose and Main Activities

The main activity of the proposed CCGT would be the generation of mid-merit power supply to the South African electricity grid. The fuel used to generate power would be natural gas, that will be delivered to site by pipeline.

1.4 Main Hazards Due to Substance and Process

The main hazards that would occur with a loss of containment of hazardous components at the proposed CCGT facility in Kempton Park include exposure to:

- Thermal radiation from fires;
- Toxic gas releases; and
- Overpressure from explosions.

1.5 Software

Physical consequences were calculated using Gexcon's RISKCURVES v. 11.5.1. All calculations were performed by Mr M P Oberholzer.

1.6 Assumptions and Limitations

The risk assessment was based on the conceptual designs of the facility, excluding the details still to be determined from the detailed designs. Furthermore, EIAs are intended to suggest mitigation which may alter the design and layout of the project. It is thus understood that detailed designs would be required to complete the project for construction.

RISCOM used the information provided and made engineering assumptions as described in the document for the purposes of compiling this quantitative risk assessment. The accuracy of the document would be limited to the available documents presented for the completion of this report. However, the inventory of hazardous goods of the facility is not expected to increase from the amounts stated in this document and despite the potential of an improved site layout, we expect the maximum impacts to be representative.

With the detailed designs, we expect additional mitigation, which should reduce the risks as recommended.

The greatest impact on accuracy would be omissions from the design presented, changes to the process, substitution of hazardous goods (typically), as required by the equipment supplier or the increase of hazardous goods inventory. These would be evaluated under the Major Hazardous Installation regulations, prior to construction.

The risk assessment excludes the following:

- Natural events, such as earthquakes and floods;
- Ecological risk assessment;
- The risk assessment of the underground pipeline leading up to the plant boundary;
- An emergency plan.

2 ENVIRONMENT

2.1 General Background

The site location for the proposed CCGT facility is at the current Kelvin Power Station, as shown in Figure 2-1.

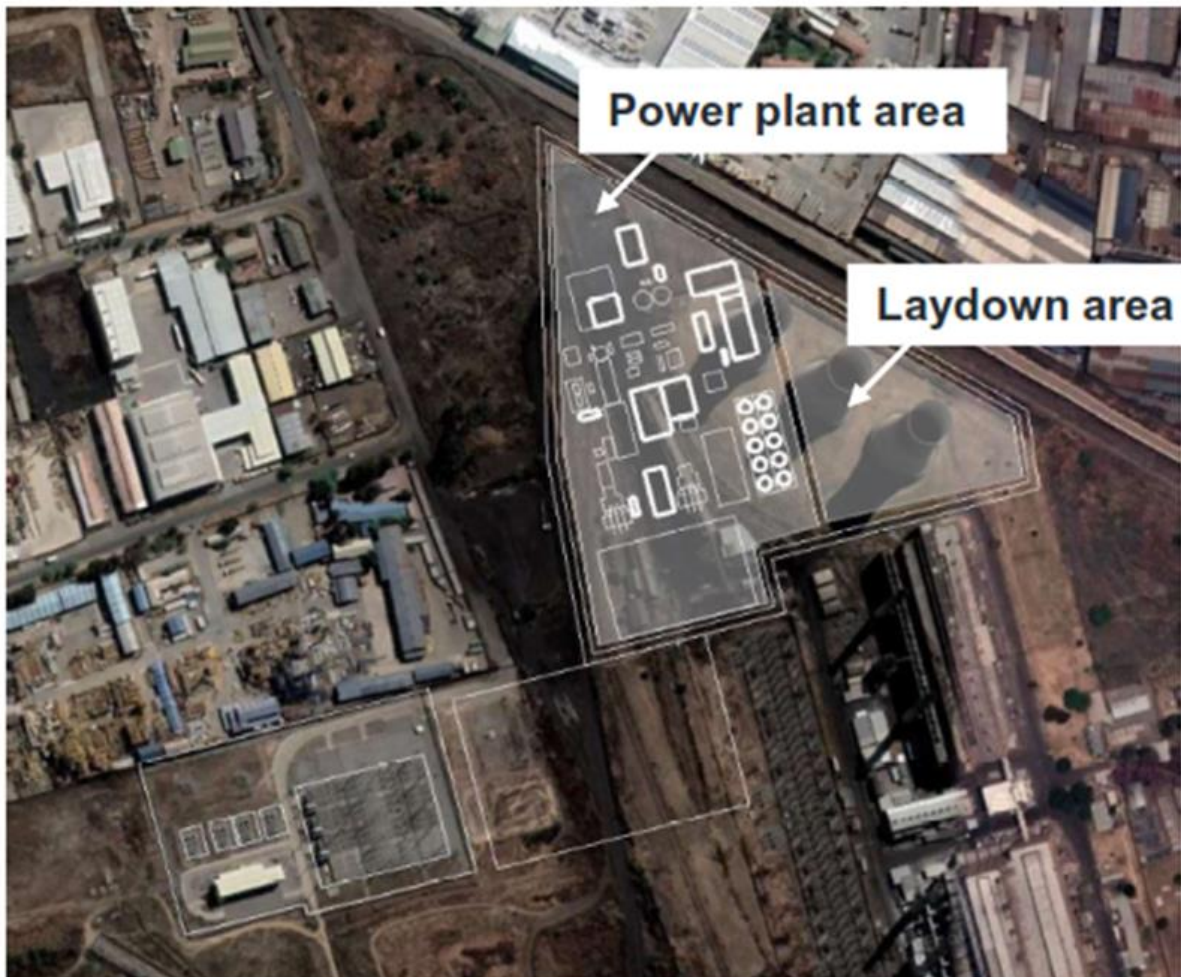


Figure 2-1: Proposed CCGT location at the Kelvin Power Station

The Kelvin Power Station has an access control point, whereby all traffic and people are controlled. Thus, all people entering the site will be limited to workers, and the general public will not have access to free movement within the zoned area.

The land use surrounding the proposed CCGT facility is shown in Figure 2-1.

The Kelvin Power Station is located between the suburbs of Kempton Park and Edenvale. The closest residential area is Cresslawn approximately 300 m east of the proposed CCGT facility.

2.2 Meteorology

Meteorological mechanisms govern dispersion, transformation and eventual removal of hazardous vapours from the atmosphere. The extent to which hazardous vapours will accumulate or disperse in the atmosphere is dependent on the degree of thermal and mechanical turbulence within the earth's boundary layer.

Dispersion comprises of vertical and horizontal components of motion. The stability and the depth of the atmosphere from the surface (known as the mixing layer) define the vertical component. The horizontal dispersion of hazardous vapours in the atmospheric boundary layer is primarily a function of the wind field. Wind speed determines both the distance of downwind transport and the rate of dilution as a result of stretching of the plume, and generation of mechanical turbulence is a function of the wind speed in combination with surface roughness. Wind direction and variability in wind direction, both determine the general path hazardous vapours will follow and the extent of crosswind spreading.

Concentration levels of hazardous vapours therefore fluctuate in response to changes in atmospheric stability, to concurrent variations in the mixing layer depth and to shifts in the wind field.

For this report, the meteorological conditions at the O R Tambo International Airport, as measured by the South African Weather Service, were used as the basis of wind speed and direction, temperature, precipitation and atmospheric humidity and stability.

2.2.1 Surface Winds

Hourly averages of wind speed and direction recorded at the O R Tambo International Airport were obtained from the South African Weather Service for the period from the 1st of January 2019 to the 31st of December 2023.

The wind roses in Figure 2-2 depicts the yearly wind speeds and directions. The calm conditions are limited below 2% with the dominant wind direction from the northwestern quadrant. High wind speeds would be rare, with medium wind speeds being the most common.

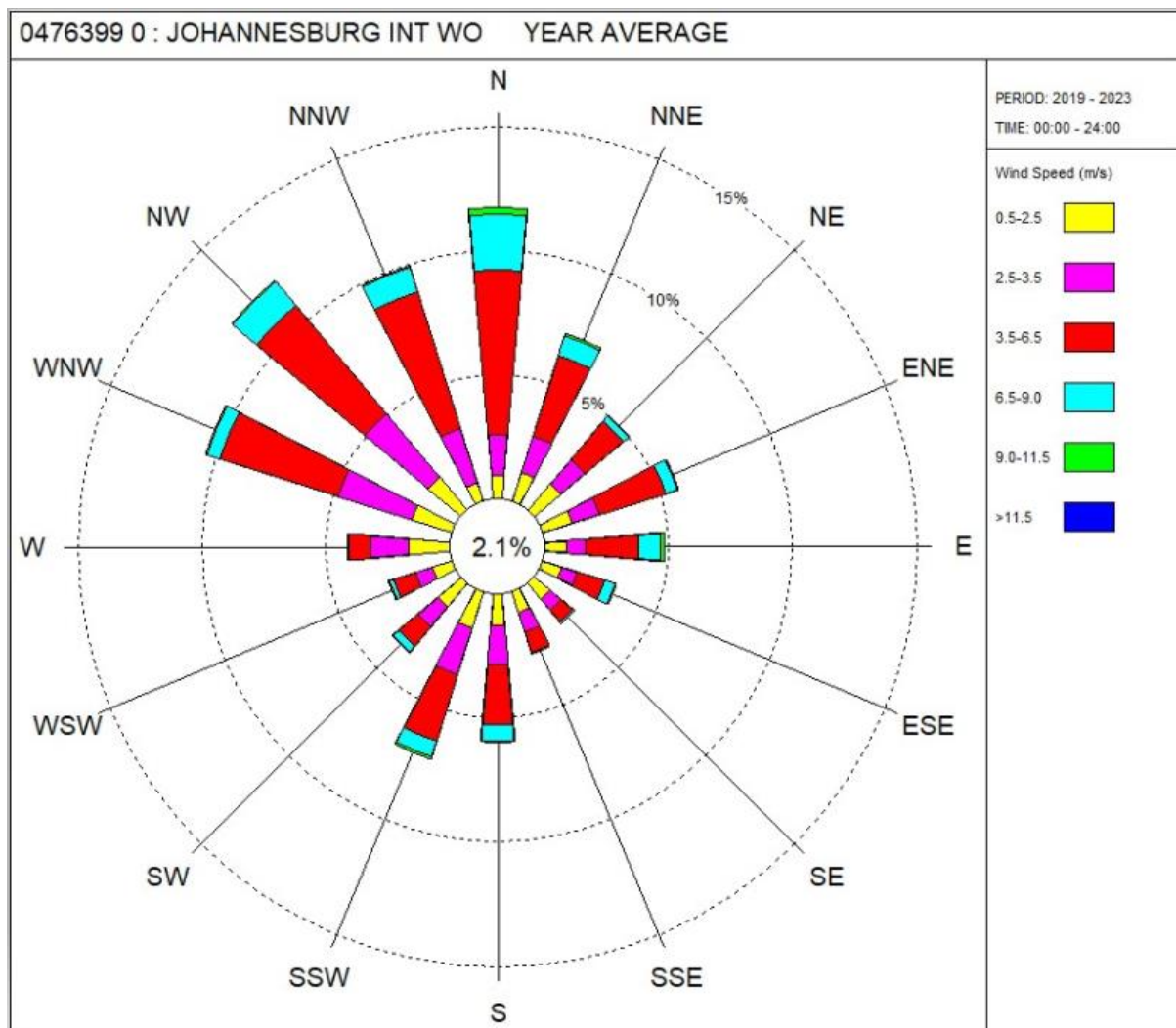


Figure 2-2: Seasonal wind speed as a function of wind direction at the O R Tambo International Airport for the period from 2019-2023

2.2.2 Precipitation and Relative Humidity

The long-term rainfall and relative humidity recorded at the O R Tambo International Airport was obtained from the South African Weather Service for the period from 1981 to 2010, as given in Table 2-1.

At the O R Tambo International Airport there is an average annual rainfall of 750 mm with the dry season ranging from April to September.

Table 2-1: Long-term rainfall and relative humidity at the O R Tambo International Airport

Month	Average Monthly Rainfall (mm)	Average Relative Humidity Monthly Minimum (%)	Average Relative Humidity Monthly Maximum (%)
January	135	57	82
February	112	50	87
March	101	50	88
April	37	51	80
May	18	33	70
June	10	33	71
July	2	39	64
August	7	37	69
September	22	31	68
October	79	45	69
November	103	53	83
December	124	53	85
Year	750	50	71

2.2.3 Temperature

The long-term temperatures recorded at the O R Tambo International Airport were obtained from the South African Weather Service for the period from 1981 to 2010, as given in Table 2-2.

The surrounding region has a temperate climate with the average daily maximum between 20°C and 30°C. Temperatures rarely extend below freezing, with the mean average of the daily temperature being above 10°C.

Table 2-2: Long-term temperatures measured at the O R Tambo International Airport

Month	Highest recorded (°C)	Average Daily Maximum (°C)	Average Daily Minimum (°C)
January	33.7	25.7	14.9
February	33.5	25.5	14.4
March	32	24.3	13.2
April	29.3	22.0	10.4
May	26.4	19.5	7.0
June	24.1	16.9	4.1
July	24.4	17.1	3.7
August	26.5	19.8	6.1
September	31.2	23.3	9.3
October	32.5	24.3	11.4
November	33.6	24.7	12.8
December	32.4	25.3	14.1
Year	33.7	22.3	10.1

2.2.4 Atmospheric Stability

Atmospheric stability is frequently categorised into one of six stability classes. These are briefly described in Table 2-3. The atmospheric stability, in combination with the wind speed, is important in determining the extent of a pollutant from a release.

A very stable atmospheric condition, typically at night, would have a low wind speed and produce the greatest endpoint for a dense gas. Conversely, a buoyant gas would have the greatest endpoint distance at a high wind speed.

Table 2-3: Classification scheme for atmospheric stability

Stability Class	Stability Classification	Description
A	Very unstable	Calm wind, clear skies, hot daytime conditions.
B	Moderately unstable	Clear skies, daytime conditions.
C	Unstable	Moderate wind, slightly overcast daytime conditions.
D	Neutral	Strong winds or cloudy days and nights.
E	Stable	Moderate wind, slightly overcast night-time conditions.
F	Very stable	Low winds, clear skies, cold night-time conditions.

The atmospheric stability for the O R Tambo International Airport, as a function of the wind class, was calculated from hourly weather values supplied by the South African Weather Service from the 1st of January 2019 to the 31st of December 2023, as given in Figure 2-3.

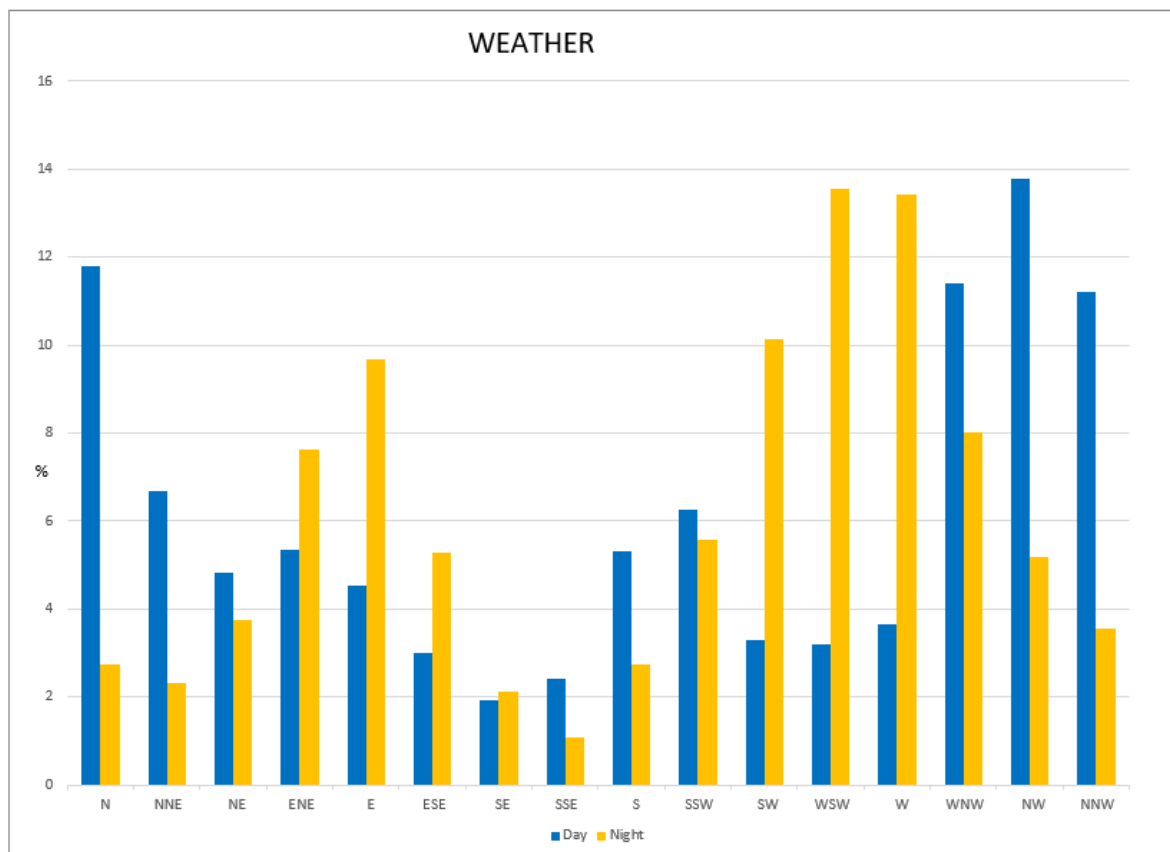


Figure 2-3: Atmospheric stability as a function of wind direction

Calculations for this risk assessment are based on six representative weather classes covering stability conditions of stable, neutral and unstable, as well as low and high wind speeds. In terms of Pasquill classes, representative conditions are given in Table 2-4.

Table 2-4: Representative weather classes

Stability Class	Wind (m/s)
B	3
D	1.5
D	5
D	9
E	5
F	1.5

As wind velocities are vector quantities (having speed and direction) and blow preferentially in certain directions, it is mathematically incorrect to give an average wind speed over 360° of wind direction; the result would be incorrect risk calculations.

It would also be incorrect to base risk calculations on one wind category, such as 1.5/F for example. In order to obtain representative risk calculations, hourly weather data for wind speed and direction was analysed over a five-year period and categorised into the six wind classes for day and night conditions and 16 wind directions. The risk was then determined by using contributions from each wind class in various wind directions.

The allocation of observations into the six weather classes is summarised in Table 2-5, with the representative weather classes given in **Figure 2-4**.

Table 2-5: Allocation of observations into six weather classes

Wind Speed	A	B	B/C	C	C/D	D	E	F
< 2.5 m/s	B 3 m/s			D 1.5 m/s			F 1.5 m/s	
2.5 - 6 m/s				D 5 m/s			E 5 m/s	
> 6 m/s				D 9 m/s				

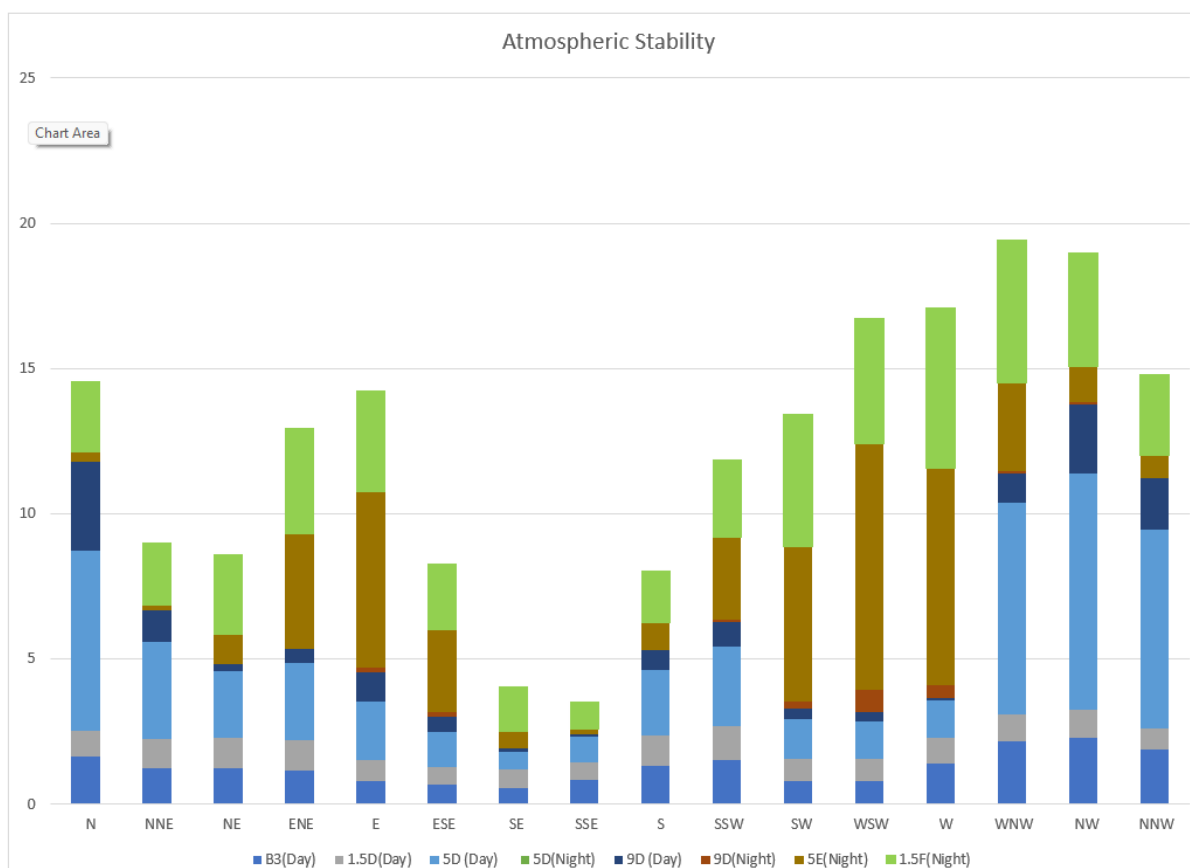


Figure 2-4: Representative weather classes for the O R Tambo International Airport

2.2.5 Meteorological Simulation Values

Default meteorological values used in simulations, based on local conditions, are given in Table 2-6.

Table 2-6: Default meteorological values used in simulations, based on local conditions

Parameter	Default Value Daytime	Default Value Night-time
Ambient temperature (°C)	22	10
Substrate/bund temperature (°C)	16	16
Water temperature (°C)	16	16
Air pressure (bar)	0.85	0.85
Humidity (%)	50	71
Fraction of a 24-hour period	0.5	0.5
Mixing height	1	1

1 Calculated in the simulation software

3 PROJECT DESCRIPTION

The proposed CCGT facility in Kempton Park is to consist offices, workshops, gas and steam turbines and associated equipment, as shown in Figure 3-1.

The site will be accessed via the main entrance of Kelvin. Thus, all unauthorised people and the general public will be excluded from the power station.

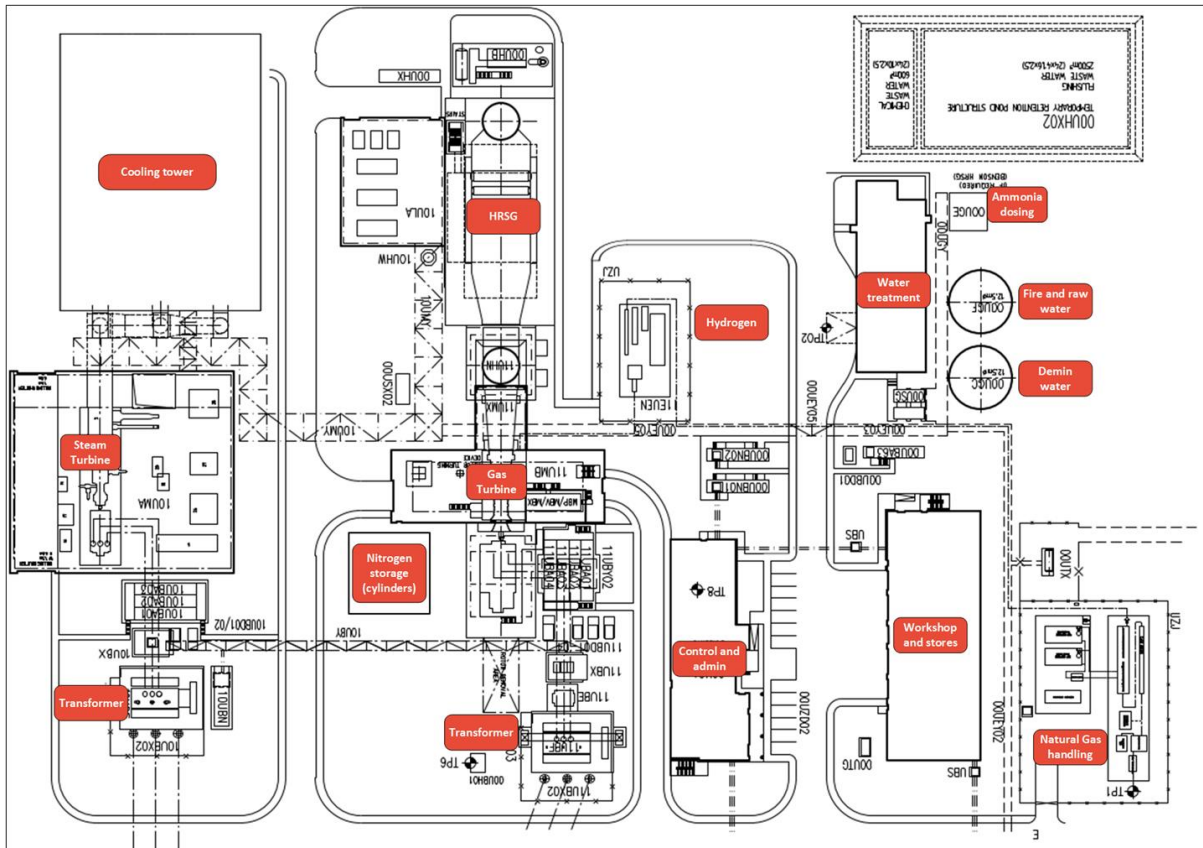


Figure 3-1: Site layout

The operation of the power station will include the following:

- Gas Turbines using natural gas as fuel to generate electricity, where compressed air is mixed with combustion fuel to produce very high temperature combustion gases. The hot combustion gases pass through the gas turbine blades, making them spin. The fast-spinning turbines drive a generator that converts a portion of the spinning energy into electricity. Each gas turbine is proposed to have a 60-metre-high by-pass stack for use during emergency events.
- During normal operations a Heat Recovery Steam Generator (HRSG) will capture heat from the combustion gas stream to produce high temperature and high-pressure dry steam, which is then supplied to a steam turbine. The combustion gases will be discharged into the atmosphere via the main exhaust stacks (60 metres high).
- The Steam turbine uses the dry steam to drive its turbine to generate electrical power. The condenser will convert exhaust steam from the steam turbine back into water through a cooling process.
- Diesel, to be used as back-up fuel, will be off-loaded by truck and stored in on-site storage tanks which will hold sufficient capacity for 8 hours of operation. Two storage tanks, each with a capacity of 5 200 m³, are planned.

- To receive natural gas via the Sasol gas pipeline network a new dedicated connection pipeline from the closest transmission pipeline branch, which runs East of the Kelvin site, will be required to bring gas to the new CCGT power plant, however, Kelvin Power will not be responsible for the construction and maintenance of this pipeline. It is noteworthy that various gas suppliers are currently being engaged for the supply of gas to the proposed CCGT Power Plant via the existing Sasol gas pipeline system. The gas pipeline will be separately authorized.

3.1 Project Description

The project will consist of up to 3 CCGTs used to produce a nominal capacity of 600 MW power from natural gas (in either liquid or gas forms) or a mixture of natural gas and hydrogen (in a proportion scaling up from 30% hydrogen - H_2) as a fuel.

The process for converting the energy in a fuel into the electric power involves the creation of mechanical work, which is then transformed into the electric power by a generator. The overall efficiency of the conversion depending on the type of fuel and the thermodynamics process used and it can be as low as 30%.

To increase the overall efficiency of electric power plants, multiple thermodynamic processes can be introduced or combined to recover and utilize the residual heat energy in hot exhaust gases. By the use of combined cycle, power plants can achieve the electrical efficiency up to 60%.

The terms “combined cycle” refers to the combining of multiple thermodynamic cycles to generate electric power. Combined cycle operation uses a heat recovery steam generator (HRSG) that captures the heat from high temperature exhaust gases to produce steam, which is then supplied to a steam turbine to generate additional electric power. The process for creating steam to produce work using a steam turbine is based on the Rankine cycle.

The most common type of combined cycle power plant utilizes gas turbines and is called a combined cycle gas turbine (CCGT) plant. Because gas turbines have low efficiency in simple cycle operation and the output produced by the steam turbine accounts for about half of the CCGT plant output.

The simplified schematic of the CCGT power plant is shown in Figure 3-2.

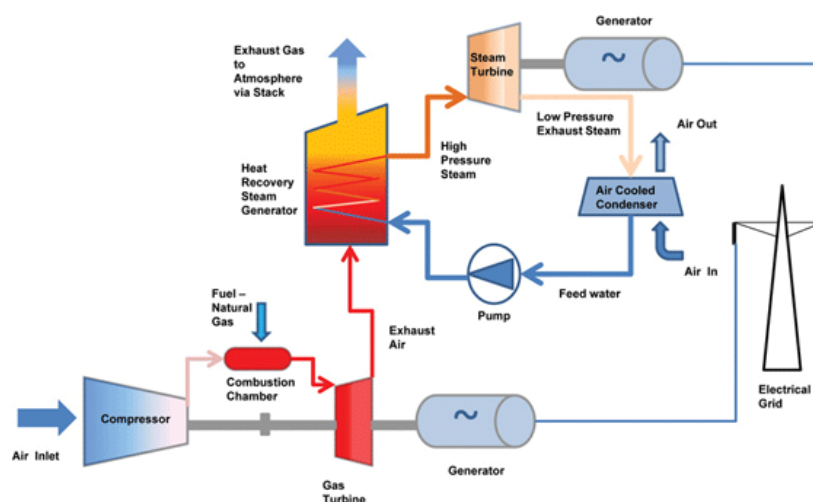


Figure 3-2: Simplified schematic of a CCGT power plant

3.2 Fuel and Process Chemicals

3.2.1 Natural Gas

Natural gas would be used to fuel the gas turbines. The gas will be supplied via a pipeline. This study assumes a gas supply pressure of 46 bar. No storage of natural gas would be provided.

3.2.2 Diesel

A 24 m³ diesel storage tank would be provided for emergency power.

3.2.3 Hydrogen

One hydrogen trailer has been provided in the design. The trailer is assured to be that of a standard hydrogen trailer of 190 kg hydrogen inventory with a storage pressure at 226 bar(g).

3.2.4 Ammonia

Ammonia would be used to adjust the pH of the boiler water feed. The size and storage details of the ammonia has not been provided. However, a 10 m³ ammonia tank was assumed.

3.2.5 Nitrogen

Nitrogen would be required to purge natural gas in pipelines and equipment prior to conducting maintenance.

The nitrogen designs have not been specified at this stage of the project.

4 METHODOLOGY

Risk assessments done in accordance with the MHI regulations are required to be conducted according to SANS 1461 (2018). This standard is specific to the MHI risk assessment that is required to be done prior to construction and includes elements that are not usually available at the preparation stage of a project, such as emergency plans and mitigation suggested during the EIA process.

SANS 1461 (2018) is based on RIVM (2009) for process plants. The latter standards describe the minimum scenarios to be included in the assessment, as well as the assumptions to be used. As full compliance of SANS 1461 (2018) cannot be achieved within the NEMA legislative framework, general compliance of the aforementioned standards at this stage would be applicable and briefly described in the sections below. This general compliance assessment constitutes a quantitative risk assessment (QRA).

The QRA process is summarised with the following steps:

1. Identification of components that are flammable, toxic, reactive or corrosive and that have potential to result in a major incident from fires, explosions or toxic releases;
2. Development of accidental loss of containment (LOC) scenarios for equipment containing hazardous components (including release rate, location and orientation of release);
3. For each incident developed in Step 2, determination of consequences (such as thermal radiation, domino effects, toxic-cloud formation and so forth);
4. For scenarios with off-site consequences (greater than 1% fatality off-site), calculation of maximum individual risk (MIR), taking into account all generic failure rates, initiating events (such as ignition), meteorological conditions and lethality.

4.1 Hazard Identification

The first step in any risk assessment is to identify all hazards. The merit of including a hazard for further investigation is then determined by how significant it is, normally by using a cut-off or threshold value.

Once a hazard has been identified, it is necessary to assess it in terms of the risk it presents to the employees and the neighbouring community. In principle, both probability and consequence should be considered but there are occasions where, if either the probability or the consequence can be shown to be sufficiently low or sufficiently high, decisions can be made based on just one factor.

During the hazard identification component of the report, the following considerations are taken into account:

- Chemical identities;
- Location of on-site installations that use, produce, process, transport or store hazardous components;
- Type and design of containers, vessels or pipelines;
- Quantity of material that could be involved in an airborne release;
- Nature of the hazard most likely to accompany hazardous materials spills or releases, e.g., airborne toxic vapours or mists, fires or explosions, large quantities to be stored and certain handling conditions of processed components.

The evaluation methodology assumes that the facility will perform as designed in absence of unintended events, such as component and material failures of equipment, human errors, external events and process unknowns.

4.1.1 Notifiable Substances

The General Machinery Regulation 8 and its Schedule A on notifiable substances, requires any employer who has a substance equal to or exceeding the quantity listed in the regulation to notify the divisional director. A site is classified as a Major Hazard Installation if it contains one or more notifiable substances, or if the off-site risk is sufficiently high. The latter can only be determined from a quantitative risk assessment.

The notifiable threshold for ammonia is listed as 20 tonne in a single vessel. As the proposed installation should not exceed the threshold limit, ammonia will not be classified as a notifiable substance.

4.1.2 Major Hazard Establishment

According to chapter 3 the “Classification of pipelines as major hazard establishment” of Major Hazard Installation Regulations, 2022:

A pipeline is considered an establishment if it contains a fluid which is or is to be conveyed in a pipeline as a gas which is flammable in air (is applicable to flammable gases conveyed as a gas. In such cases the additional duties only apply when the flammable gas is conveyed at a pressure in excess of 8 bars absolute. This covers such fluids as methane, butane and propane).

4.1.3 Substance Hazards

All components on site were assessed for potential hazards according to the criteria discussed in this section.

4.1.3.1 Chemical Properties

A short description of bulk hazardous components to be stored on, produced at or delivered to site is given in the following subsections. The material safety data sheets (MSDSs) of the respective materials are not available at this stage.

- **Ammonia**

Ammonia is a colourless gas with a pungent and suffocating odour. It liquefies easily under pressure, with a normal boiling point of -33°C. Although classified as a non-flammable gas, it will burn in 16–25% vapour concentrations in air when exposed to open flames.

It is incompatible with certain materials. It is corrosive to copper, brass, silver, zinc and galvanized steel. Contact with strong oxidizers can result in fires and explosions. It forms explosive products when in contact with calcium hypochlorite (household) bleaches, halogens, gold, mercury and silver. Heat is generated when ammonia dissolves in water. At high

temperatures, ammonia emits hydrogen and nitrogen. Products of combustion include nitrogen and water, which are harmless to life and the environment.

The effects of anhydrous ammonia upon the human body vary with the size and weight of the subject and to a lesser extent temperature and humidity.

Contact with liquid ammonia can cause frostbite. Ammonia is soluble in water, forming a corrosive liquid. It is toxic if swallowed or inhaled and can irritate or burn skin, eyes, the nose or the throat at levels as low as 35 ppm but normally at 100–125 ppm, through inhalation or direct contact. At 700 ppm it can cause serious and permanent injury with extreme rapidity.

Upon contact with moist mucosal membranes (such as those in the skin, eyes and respiratory tract), ammonia reacts with water to form a strong alkali, ammonium hydroxide. This causes severe damage to the surface of tissues, thereby exposing more tissue to the effects of the alkali. Symptoms are rapid on contact due to the high-water solubility of ammonia and include immediate burning of the eyes, nose and throat and coughing and bronchospasm with wheezing and pulmonary oedema (fluid around the lungs).

Massive exposures can override the absorptive surface area of the upper respiratory tract and result in extensive injury to the lower airways and lung tissue.

There have been a number of major accidents involving ammonia involving storage tanks and pipelines as well as ammonia transported on trucks, railcars and ships.

The worst incident occurred in 1973 in Potchefstroom, South Africa, where a failure of an ammonia tank released approximately 39 t killing 18 people.

There have been a number of nonfatal releases of ammonia. A release of about 600 t of ammonia occurred from a pipeline in Floral, Arkansas, in 1971 and resulted in a fish kill but no injuries. In another incident, 230 t of ammonia was released from a pipeline at McPherson, Kansas, without fatalities.

- **Diesel**

Diesel is a hydrocarbon mixture with variable composition, with a boiling-point range of between 252°C and 371°C. It is a pale-yellow liquid with a petroleum odour. Due to the flash point of diesel between 38°C and 65°C, this material is not considered highly flammable but will readily ignite under suitable conditions.

Diesel is stable under normal conditions. It will react with strong oxidising agents and nitrate compounds. This reaction may cause fires and explosions.

Diesel is not considered a toxic material. Contact with vapours may result in slight irritation to nose, eyes and skin. Vapours may cause headache, dizziness, loss of consciousness or suffocation as well as lung irritation with coughing, gagging, dyspnoea, substernal distress and rapidly developing pulmonary oedema.

If swallowed, diesel may cause nausea or vomiting, swelling of the abdomen, headache, CNS depression, coma and death.

The long-term effects of diesel exposure have not been determined. However, this may affect the lungs and may cause the skin to dry out and become cracked.

Diesel floats on water and can result in environmental hazards with large spills into waterways. It is harmful to aquatic life in high concentrations.

- **Hydrogen**

Hydrogen is a colourless odourless gas that is flammable over a wide range of air or vapour concentrations. The vapour forms an explosive mixture with air. Vapours or gases may travel considerable distances to an ignition source and flash back.

Leaking hydrogen may ignite in the absence of any normally apparent source of ignition and, if so, burns with a practically invisible flame that can instantly injure anyone coming in contact with it. Hydrogen gas is very light and rises rapidly in the air. Concentrations may collect in the upper portions of buildings. The liquid can solidify air and may create an explosion hazard. The very cold gas, as it comes from the liquid, is slightly heavier than air and may remain near ground level until it warms up. Fog formed when the cold gas contacts atmospheric moisture indicates where the gas is spreading but flammable mixtures may exist beyond the visible fog. Explosive atmospheres may linger. Under prolonged exposure to fire or intense heat the containers may rupture violently and rocket.

It is incompatible with oxygen, oxidising agents, air, lithium and halogens. It may react explosively at elevated temperatures or with heating, alkali metals, halogens, oxygen, oxidizers, oxides, ozone, chlorides, dichlorides and trichlorides of nitrogen and unsaturated hydrocarbons. Divided platinum and some other metals will cause a mixture of hydrogen and oxygen to explode at ordinary temperatures. Embrittlement of steel and other metals such as nickel and copper-nickel alloys will occur at ambient temperatures on exposure to the gas at high pressures.

It is not toxic but is a simple asphyxiant by the displacement of oxygen in the air. Exposure to the liquid may result in frostbite.

- **Natural Gas**

The composition of natural gas is primarily methane ($\pm 95\%$ v/v), with other components including ethane, propane and nitrogen.

Given the flammable and potentially explosive nature of natural gas, fires and vapour cloud explosions represent the primary hazards associated with transfer of the gas. The gas is a fire and explosion hazard when it is exposed to heat and flame. The lower explosive limit (LEL) is 5% v/v (meaning 5% gas to 95% air, measured by volume) and the upper explosive limit (UEL) is 15% v/v. In unconfined atmospheric conditions, the likelihood of an explosion is expected to be small.

It is not compatible with strong oxidants and could result in fires and explosions in the presence of such materials.

It is nontoxic and would be considered as an asphyxiant only. Chronic and long-term effects are low and are not listed.

4.1.3.2 Corrosive Liquids

Corrosive liquids considered under this subsection, are those components that have a low or high pH and that may cause burns if they come into contact with people or may attack and cause failure of equipment.

Ammonia would be considered corrosive, but is analysed as a toxic component.

4.1.3.3 Reactive Components

Reactive components are components that when mixed or exposed to one another react in a way that may cause a fire, explosion or release a toxic component.

All components to be stored on, produced at or delivered to site are considered thermally stable in atmospheric conditions. The reaction with air is covered under the subsection dealing with ignition probabilities.

4.1.3.4 Flammable and Combustible Components

Flammable and combustible components are those that can ignite and give a number of hazardous effects, depending on the nature of the component and conditions. These effects may include pool fires, jet fires and flash fires as well as explosions and fireballs.

The flammable and combustible components to be stored on, produced at or delivered to site, are listed in Table 4-1. These components have been analysed for fire and explosion risks.

Table 4-1: Flammable and combustible components to be stored on, produced at or delivered to site

Component	Flashpoint (°C)	Boiling Point (°C)	LFL (vol. %)	UFL (vol. %)
Natural gas (methane)	-188	-161	5	15

4.1.4 Physical Properties

For this study, natural gas was modelled as a pure component, as given in Table 4-2. The physical properties used in the simulations were based on the DIPPR¹ data base, which are preloaded in the simulation software.

Table 4-2: Representative components

Component	Modelled as
Natural gas	Methane

1 Design Institute for Physical Properties

4.1.5 Components Excluded from the Study

Components excluded from the study, are listed in Table 4-3.

Table 4-3: Components excluded from the study

Component	Inventory	Reasons for Exclusion
Nitrogen	Portable cylinders	Will only be brought on site when maintenance would be required and would be in cylinders.
Diesel	Tank	Considered to be insignificant storage capacity
Lube oil	Small, used to lubricate the gensets	High flash point >100°C.

4.2 Physical and Consequence Modelling

In order to establish which impacts follow an accident, it is first necessary to estimate the physical process of the spill (i.e., rate and size), spreading of the spill, evaporation from the spill, subsequent atmospheric dispersion of the airborne cloud and, in the case of ignition, the burning rate and resulting thermal radiation from a fire and the overpressures from an explosion.

The second step is then to estimate the consequences of a release on humans, fauna, flora and structures in terms of the significance and extent of the impact in the event of a release. The consequences could be due to toxic or asphyxiant vapours, thermal radiation or explosion overpressures. They may be described in various formats.

The simplest methodology would show a comparison of predicted concentrations, thermal radiation or overpressures to short-term guideline values.

In a different but more realistic fashion, the consequences may be determined by using a dose-response analysis. Dose-response analysis aims to relate the intensity of the phenomenon that constitutes a hazard to the degree of injury or damage that it can cause. Probit analysis is possibly the method mostly used to estimate probability of death, hospitalisation or structural damage. The probit is a lognormal distribution and represents a measure of the percentage of the vulnerable resource that sustains injury or damage. The probability of injury or death (i.e., the risk level) is in turn estimated from this probit (risk characterisation).

Consequence modelling gives an indication of the extent of the impact for selected events and is used primarily for emergency planning. A consequence that would not cause irreversible injuries would be considered insignificant, and no further analysis would be required. The effects from major incidents are summarised in the following subsections.

4.2.1 Fires

Combustible and flammable components within their flammable limits may ignite and burn if exposed to an ignition source of sufficient energy. On process plants, releases with ignition normally occur as a result of a leakage or spillage. Depending on the physical properties of the component and the operating parameters, combustion may take on a number of forms, such as pool fires, jet fires, flash fires and so forth.

4.2.1.1 Thermal Radiation

The effect of thermal radiation is very dependent on the type of fire and duration of exposure. Certain codes, such as the American Petroleum Institute API 520 and API 2000 codes, suggest values for the maximum heat absorbed by vessels to facilitate adequate relief designs in order to prevent failure of the vessel. Other codes, such as API 510 and the British Standards BS 5980 code, give guidelines for the maximum thermal radiation intensity and act as a guide to equipment layout, as shown in Table 4-4.

The effect of thermal radiation on human health has been widely studied, relating injuries to the time and intensity of exposure.

Table 4-4: Thermal radiation guidelines (BS 5980 of 1990)

Thermal Radiation Intensity (kW/m ²)	Limit
1.5	Will cause no discomfort for long exposure.
2.1	Sufficient to cause pain if unable to reach cover within 40 seconds.
4.5	Sufficient to cause pain if unable to reach cover within 20 seconds.
12.5	Minimum energy required for piloted ignition of wood and melting of plastic tubing.
25	Minimum energy required to ignite wood at indefinitely long exposures.
37.5	Sufficient to cause serious damage to process equipment.

For pool fires, jet fires and flash fires CPR 18E (Purple Book; 1999) suggests the following thermal radiation levels be reported:

- 4 kW/m², the level that glass can withstand, preventing the fire entering a building, and that should be used for emergency planning;
- 10 kW/m², the level that represents the 1% fatality for 20 seconds of unprotected exposure and at which plastic and wood may start to burn, transferring the fire to other areas;
- 35 kW/m², the level at which spontaneous ignition of hair and clothing occurs, with an assumed 100% fatality, and at which initial damage to steel may occur.

4.2.1.2 Bund and Pool Fires

Pool fires, either tank or bund fires, consist of large volumes of a flammable liquid component burning in an open space at atmospheric pressure.

The flammable component will be consumed at the burning rate, depending on factors including prevailing winds. During combustion, heat will be released in the form of thermal radiation. Temperatures close to the flame centre will be high but will reduce rapidly to tolerable temperatures over a relatively short distance. Any building or persons close to the fire or within the intolerable zone, will experience burn damage with severity depending on the distance from the fire and time exposed to the heat of the fire.

In the event of a pool fire, the flames will tilt according to the wind speed and direction. The flame length and tilt angle affect the distance of thermal radiation generated.

4.2.1.3 Jet Fires

Jet fires occur when a flammable component which is released with a high exit velocity, ignites.

In process industries, this may be due to design (such as flares) or due to accidental releases. Ejection of a flammable component from a vessel, pipe or pipe flange may give rise to a jet fire and in some instances, the jet flame could have substantial 'reach'.

In modelling jet fires from punctures, the release can be considered to be steady-state. For underground modelling, consequence model considers a vertical jet flame at ground level, with wind tilt created by the current wind velocity. Above ground pipelines are modelled as horizontal releases at the release height.

Depending on wind speed, the flame may tilt and impinge on other pipelines, equipment or structures. The thermal radiation from these fires may cause injury to people or damage equipment some distance away from the source of the flame.

4.2.1.4 Fireball

A fireball occurs with the immediate ignition of a large gas release forming a mushroom-shaped cap that is fed from below by the established part of the fire, lasts typically for up to 30 seconds (depending on pipeline diameter and initial pressure).

4.2.1.5 Flash Fires

A loss of containment of a flammable component may mix with air, forming a flammable mixture. The flammable cloud would be defined by the lower flammable limit (LFL) and the upper flammable limit (UFL). The extent of the flammable cloud would depend on the quantity of the released and mixed component, physical properties of the released component, wind speed and weather stability.

An ignition within a flammable cloud can result in an explosion if the front is propagated by pressure. If the front is propagated by heat, then the fire moves across the flammable cloud at the flame velocity and is called a flash fire. Flash fires are characterised by low overpressure, and injuries are caused by thermal radiation. The effects of overpressure due

to an exploding cloud are covered in the subsection dealing with vapour cloud explosions (VCEs).

A flash fire would extend to the lower flammable limit; however, due to the formation of pockets, it could extend beyond this limit to the point defined as the $\frac{1}{2}$ LFL. It is assumed that people within the flash fire would experience lethal injuries, while people outside of the flash fire would remain unharmed. The $\frac{1}{2}$ LFL is used for emergency planning to evacuate people to a safe distance in the event of a release.

4.2.2 Explosions

The concentration of a flammable component would decrease from the point of release to below the lower explosive limits (LEL), at which concentration the component can no longer ignite. The sudden detonation of an explosive mass would cause overpressures that could result in injury or damage to property.

Such an explosion may give rise to any of the following effects:

- Blast damage;
- Thermal damage;
- Missile damage;
- Ground tremors;
- Crater formation;
- Personal injury.

Obviously, the nature of these effects depends on the pressure waves and the proximity to the actual explosion. Of concern in this investigation are the 'far distance effects', such as limited structural damage and the breakage of windows, rather than crater formations.

Table 4-5 and Table 4-6 give a more detailed summary of the damage produced by an explosion due to various overpressures.

CPR 18E (Purple Book; 1999) suggests the following overpressures be determined:

- 0.03 bar overpressure, corresponding to the critical overpressure causing windows to break;
- 0.1 bar overpressure, corresponding to 10% of the houses being severely damaged and a probability of death indoors equal to 0.025:
 - No lethal effects are expected below 0.1 bar overpressure on unprotected people in the open;
- 0.3 bar overpressure, corresponding to structures being severely damaged and 100% fatality for unprotected people in the open;
- 0.7 bar overpressure, corresponding to an almost entire destruction of buildings.

Table 4-5: Summary of consequences of blast overpressure (Clancey 1972)

Pressure (Gauge)		Damage
Psi	kPa	
0.02	0.138	Annoying noise (137 dB), if of low frequency (10 – 15 Hz).
0.03	0.207	Occasional breaking of large glass windows already under strain.
0.04	0.276	Loud noise (143 dB); sonic boom glass failure.
0.1	0.69	Breakage of small under strain windows.
0.15	1.035	Typical pressure for glass failure.
0.3	2.07	'Safe distance' (probability 0.95; no serious damage beyond this value); missile limit; some damage to house ceilings; 10% window glass broken.
0.4	2.76	Limited minor structural damage.
0.5–1.0	3.45–6.9	Large and small windows usually shattered; occasional damage to window frames.
0.7	4.83	Minor damage to house structures.
1.0	6.9	Partial demolition of houses, made uninhabitable.
1.0–2.0	6.9–13.8	Corrugated asbestos shattered; corrugated steel or aluminium panels, fastenings fail, followed by buckling; wood panels (standard housing) fastenings fail, panels blown in.
1.3	8.97	Steel frame of clad building slightly distorted.
2.0	13.8	Partial collapse of walls and roofs of houses.
2.0–3.0	13.8–20.7	Concrete or cinderblock walls (not reinforced) shattered.
2.3	15.87	Lower limit of serious structural damage.
2.5	17.25	50% destruction of brickwork of house.
3.0	20.7	Heavy machines (1.4 t) in industrial building suffered little damage; steel frame building distorted and pulled away from foundations.
3.0–4.0	20.7–27.6	Frameless, self-framing steel panel building demolished.
4.0	27.6	Cladding of light industrial buildings demolished.
5.0	34.5	Wooden utilities poles (telegraph, etc.) snapped; tall hydraulic press (18 t) in building slightly damaged.
5.0–7.0	34.5–48.3	Nearly complete destruction of houses.
7.0	48.3	Loaded train wagons overturned.
7.0–8.0	48.3–55.2	Brick panels (20 – 30 cm) not reinforced fail by shearing or flexure.
9.0	62.1	Loaded train boxcars completely demolished.
10.0	69.0	Probable total destruction buildings; heavy (3 t) machine tools moved and badly damaged; very heavy (12 000 lb. / 5443 kg) machine tools survived.
300	2070	Limit of crater lip.

Table 4-6: Damage caused by overpressure effects of an explosion (Stephens 1970)

Equipment	Overpressure (psi)																								
	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6	6.5	7	7.5	8	8.5	9	9.5	10	12	14	16	18	20
Control house steel roof	A	C	V				N																		
Control house concrete roof	A	E	P	D			N																		
Cooling tower	B			F			O																		
Tank: cone roof		D				K							U												
Instrument cubicle			A			LM						T													
Fire heater				G	I					T															
Reactor: chemical				A				I				P						T							
Filter				H					F									V			T				
Regenerator						I				IP					T										
Tank: floating roof						K							U												D
Reactor: cracking							I							I							T				
Pine supports							P					SO													
Utilities: gas meter									Q																
Utilities: electric transformer									H					I							T				
Electric motor										H								I							V
Blower										Q											T				
Fractionation column											R			T											
Pressure vessel horizontal												PI						T							
Utilities: gas regulator												I								MQ					
Extraction column													I							V	T				
Steam turbine															I						M	S			V
Heat exchanger															I			T							
Tank sphere																I						I	T		
Pressure vessel vertical																					I	T			
Pump																					I		Y		

A

B

C

D

E

F

G

H

I

J

K

L

M

N

O

P

Q

R

S

T

U

V

Windows and gauges break

Louvers fall at 0.3–0.5 psi

Switchgear is damaged from roof collapse

Roof collapses

Instruments are damaged

Inner parts are damaged

Bracket cracks

Debris-missile damage occurs

Unit moves and pipes break

Bracing fails

Unit uplifts (half filled)

Power lines are severed

Controls are damaged

Block wall fails

Frame collapses

Frame deforms

Case is damaged

Frame cracks

Piping breaks

Unit overturns or is destroyed

Unit uplifts (0.9 filled)

Unit moves on foundations

- A Windows and gauges break
- B Louvers fall at 0.3–0.5 psi
- C Switchgear is damaged from roof collapse
- D Roof collapses
- E Instruments are damaged
- F Inner parts are damaged
- G Bracket cracks
- H Debris-missile damage occurs
- I Unit moves and pipes break
- J Bracing fails
- K Unit uplifts (half filled)
- L Power lines are severed
- M Controls are damaged
- N Block wall fails
- O Frame collapses
- P Frame deforms
- Q Case is damaged
- R Frame cracks
- S Piping breaks
- T Unit overturns or is destroyed
- U Unit uplifts (0.9 filled)
- V Unit moves on foundations

4.2.2.1 Vapour Cloud Explosions (VCEs)

The release of a flammable component into the atmosphere could result in formation of a flash fire, as described in the subsection on flash fires, or a vapour cloud explosion (VCE). In the case of a VCE, an ignited vapour cloud between the higher explosive limits (HEL) and the lower explosive limit (LEL) could form a fireball with overpressures that could result in injury or damage to property.

4.2.2.2 Boiling Liquid Expanding Vapour Explosions (BLEVEs)

A boiling liquid expanding vapour explosion (BLEVE) can occur when a flame impinges on a pressure cylinder, particularly in the vapour space region where cooling by evaporation of the contained material does not occur; the cylinder shell would weaken and rupture with a total loss of the contents, and the issuing mass of material would burn as a massive fireball.

The major consequences of a BLEVE are intense thermal radiation from the fireball, a blast wave and propelled fragments from the shattered vessel. These fragments may be projected to considerable distances. Analyses of the travel range of fragment missiles from a number of BLEVEs suggest that the majority land within 700 m from the incident. A blast wave from a BLEVE is fairly localised but can cause significant damage to immediate equipment.

A BLEVE occurs sometime after the vessel has been engulfed in flames. Should an incident occur that could result in a BLEVE, people should be evacuated to beyond the 1% fatality line.

4.3 Risk Analysis

4.3.1 Background

It is important to understand the difference between hazard and risk.

A hazard is anything that has the potential to cause damage to life, property and the environment. Furthermore, it has constant parameters (like those of petrol, chlorine, ammonia, etc.) that pose the same hazard wherever present.

On the other hand, risk is the probability that a hazard will actually cause damage and goes along with how severe that damage will be (consequence). Risk is therefore the probability that a hazard will manifest itself. For instance, the risks of a chemical accident or spill depends upon the amount present, the process the chemical is used in, the design and safety features of its container, the exposure, the prevailing environmental and weather conditions and so on.

Risk analysis consists of a judgement of probability based on local atmospheric conditions, generic failure rates and severity of consequences, based on the best available technological information.

Risks form an inherent part of modern life. Some risks are readily accepted on a day-to-day basis, while certain hazards attract headlines even when the risk is much smaller, particularly in the field of environmental protection and health. For instance, the risk of one-in-ten-thousand chance of death per year associated with driving a car is acceptable to most people, whereas the much lower risks associated with nuclear facilities (one-in-ten-million chance of death per year) are deemed unacceptable.

A report by the British Parliamentary Office of Science and Technology (POST), entitled 'Safety in Numbers? Risk Assessment and Environmental Protection', explains how public perception of risk is influenced by a number of factors in addition to the actual size of the risk. These factors were summarised as follows in Table 4-7.

Table 4-7: Influence of public perception of risk on acceptance of that risk, based on the POST report

Control	People are more willing to accept risks they impose upon themselves or they consider to be 'natural' than to have risks imposed upon them.
Dread and Scale of Impact	Fear is greatest where the consequences of a risk are likely to be catastrophic rather than spread over time.
Familiarity	People appear more willing to accept risks that are familiar rather than new risks.
Timing	Risks seem to be more acceptable if the consequences are immediate or short term, rather than if they are delayed (especially if they might affect future generations).
Social Amplification and Attenuation	Concern can be increased because of media coverage, graphic depiction of events or reduced by economic hardship.
Trust	A key factor is how far the public trusts regulators, policy makers or industry; if these bodies are open and accountable (being honest as well as admitting mistakes and limitations and taking account of differing views without disregarding them as emotive or irrational), then the public is more likely to consider them credible.

A risk assessment should be seen as an important component of ongoing preventative action, aimed at minimising or hopefully avoiding accidents. Reassessments of risks should therefore follow at regular intervals and after any changes that could alter the nature of the hazard, so contributing to an overall prevention programme and emergency response plan of the facility. Risks should be ranked with decreasing severity and the top risks reduced to acceptable levels.

Procedures for predictive hazard evaluation have been developed for the analysis of processes when evaluating very low probability accidents with very high consequences (for which there is little or no experience) as well as more likely releases with fewer consequences (for which there may be more information available). These address both the probability of an accident as well as the magnitude and nature of undesirable consequences of that accident. Risk is usually defined as some simple function of both the probability and consequence.

4.3.2 Predicted Risk

Physical and consequence modelling addresses the impact of a release of a hazardous component without taking into account probability of occurrence. This merely illustrates the significance and the extent of the impact in the event of a release. Modelling should also analyse cascading or knock-on effects due to incidents in the facility and the surrounding industries and suburbs.

During a risk analysis, the likelihood of various incidents is assessed, the consequences calculated and finally the risk for the facility is determined.

4.3.3 Generic Equipment Failure Scenarios

In order to characterise various failure events and assign a failure frequency, fault trees were constructed starting with a final event and working from the top down to define all initiating events and frequencies. Unless otherwise stated, analysis was completed using published failure rate data (RIVM 2009). Equipment failures can occur in tanks, pipelines and other items handling hazardous chemical components. These failures may result in:

- Release of combustible, flammable and explosive components with fires or explosions upon ignition.

4.3.3.1 Storage Vessels

Scenarios involving storage vessels can include catastrophic failures that would lead to leakage into the bund with a possible bund fire. A tank-roof failure could result in a possible tank-top fire. The fracture of a nozzle or transfer pipeline could also result in leakage into the bund.

Typical failure frequencies for atmospheric and pressure vessels are listed, respectively, in Table 4-8 and Table 4-9.

Table 4-8: Failure frequencies for atmospheric vessels

Event	Leak Frequency (per item per year)
Small leaks	1×10^{-4}
Severe leaks	3×10^{-5}
Catastrophic failure	5×10^{-6}

Table 4-9: Failure frequencies for pressure vessels

Event	Failure Frequency (per item per year)
Small leaks	1×10^{-5}
Severe leaks	5×10^{-7}
Catastrophic failure	5×10^{-7}

4.3.3.2 Transport and Process Piping

Piping may fail as a result of corrosion, erosion, mechanical impact damage, pressure surge (water hammer) or operation outside the design limitations for pressure and temperature. Failures caused by corrosion and erosion usually result in small leaks, which are easily detected and corrected quickly. For significant failures, the leak duration may be from 10 – 30 minutes before detection.

Generic data for leak frequency for process piping is generally expressed in terms of the cumulative total failure rate per year for a 10 m section of pipe for each pipe diameter. Furthermore, failure frequency normally decreases with increasing pipe diameter. Scenarios and failure frequencies for a pipeline apply to pipelines with connections, such as flanges, welds and valves.

The failure data given in Table 4-10 represents the total failure rate, incorporating all failures of whatever size and due to all probable causes. These frequencies are based on an assumed environment where no excessive vibration, corrosion, erosion or thermal cyclic stresses are expected. For incidents causing significant leaks (such as corrosion), the failure rate will be increased by a factor of 10.

Table 4-10: Failure frequencies for process pipes

Description	Frequencies of Loss of Containment for Process Pipes (per meter per year)	
	Full Bore Rupture	Leak
Nominal diameter < 75 mm	1×10^{-6}	5×10^{-6}
75 mm < nominal diameter < 150 mm	3×10^{-7}	2×10^{-6}
Nominal diameter > 150 mm	1×10^{-7}	5×10^{-7}

4.3.3.3 Pumps and Compressors

Pumps can be subdivided roughly into two different types, reciprocating pumps and centrifugal pumps. This latter category can be further subdivided into canned pumps (sealless pumps) and gasket (pumps with seals). A canned pump can be defined as an encapsulated pump where the process liquid is located in the space around the rotor (impeller), in which case gaskets are not used.

Compressors can also be subdivided roughly into reciprocating compressors and centrifugal compressors.

Failure rates for pumps and compressors, are given in Table 4-11 and Table 4-12.

Table 4-11: Failure frequency for centrifugal pumps and compressors

Event	Canned (No Gasket) Frequency (per annum)	Gasket Frequency (per annum)
Catastrophic failure	1.0×10^{-5}	1.0×10^{-4}
Leak (10% diameter)	5.0×10^{-5}	4.4×10^{-3}

Table 4-12: Failure frequency for reciprocating pumps and compressors

Event	Frequency (per annum)
Catastrophic failure	1.0×10^{-4}
Leak (10% diameter)	4.4×10^{-3}

4.3.3.4 Loading and Offloading

Loading can take place from a storage vessel to a transport unit (road tanker, tanker wagon or ship), or from a transport unit to a storage vessel. The failure frequencies for loading and offloading arms, are given in Table 4-13.

Table 4-13: Failure frequencies for loading and offloading arms and hoses

Event	Frequency (per hour)	
	Loading and Offloading Arms	Loading and Offloading Hoses
Rupture	3×10^{-8}	4×10^{-6}
Leak with effective diameter at 10% of nominal diameter to max. 50 mm	3×10^{-7}	4×10^{-5}

4.3.3.5 Human Failure

Human error and failure can occur during any life cycle or mode of operation of a facility. Human failure can be divided into the following categories:

- Human failure during design, construction and modification of the facility;
- Human failure during operation and maintenance;
- Human failure due to errors of management and administration.

Human failure during design, construction and modification is part of the generic failure given in this subsection. Human failure due to errors of organisation and management are influencing factors. Some of the types of tasks that have been evaluated for their rates of human failure are given in Table 4-14.

Table 4-14: Human failure rates of specific types of tasks (CPR 12E 2005; Red Book)

Tasks	Human Failure (events per year)
Totally unfamiliar, performed at speed with no real idea of likely consequences.	0.55
Failure to carry out rapid and complex actions to avoid serious incident such as an explosion.	0.5
Complex task requiring high level of comprehension and skill.	0.16
Failure to respond to audible alarm in control room within 10 minutes.	1.0×10^{-1}
Failure to respond to audible alarm in quiet control room by some more complex action such as going outside and selecting one correct value among many.	1.0×10^{-2}
Failure to respond to audible alarm in quiet control room by pressing a single button.	1.0×10^{-3}
Omission or incorrect execution of step in a familiar start-up routine.	1.0×10^{-3}
Completing a familiar, well-designed, highly-practiced, routine task occurring several times per hour, performed to highest possible standards by a highly-motivated, highly-trained and experienced person totally aware of implications of failures, with time to correct potential error but without the benefit of significant job aids.	4.0×10^{-4}

4.3.3.6 Ignition Probability of Flammable Gases and Liquids

Estimation of probability of an ignition is a key step in assessment of risk for installations where flammable liquids or gases are stored. There is a reasonable amount of data available relating to characteristics of ignition sources and effects of release type and location.

Probability of ignition for stationary installations, is given in Table 4-15 (along with classification of flammable substances in Table 4-16). These can be replaced with ignition probabilities related to surrounding activities. For example, probability of a fire from a flammable release at an open flame would increase to a value of 1.

Table 4-15: Probability of direct ignition for stationary installations (RIVM 2009)

Substance Category	Source-Term Continuous	Source-Term Instantaneous	Probability of Direct Ignition
Category 0 Average to high reactivity	< 10 kg/s	< 1000 kg	0.2
	10 – 100 kg/s	1000 – 10 000 kg	0.5
	> 100 kg/s	> 10 000 kg	0.7
Category 0 Low reactivity	< 10 kg/s	< 1000 kg	0.02
	10 – 100 kg/s	1000 – 10 000 kg	0.04
	> 100 kg/s	> 10 000 kg	0.09
Category 1	All flow rates	All quantities	0.065
Category 2	All flow rates	All quantities	0.0043 ¹
Category 3 Category 4	All flow rates	All quantities	0

Table 4-16: Classification of flammable substances

Substance Category	Description	Limits
Category 0	Extremely flammable	Liquids, substances and preparations that have a flashpoint lower than 0°C and a boiling point (or the start of the boiling range) less than or equal to 35°C Gaseous substances and preparations that may ignite at normal temperature and pressure when exposed to air.
Category 1	Highly flammable	Liquids, substances and preparations that have a flashpoint of below 21°C.
Category 2	Flammable	Liquids, substances and preparations that have a flashpoint equal to 21°C and less than 55°C.
Category 3		Liquids, substances and preparations that have a flashpoint greater than 55°C and less than or equal to 100°C.
Category 4		Liquids, substances and preparations that have a flashpoint greater than 100°C.

¹ This value is taken from the CPR 18E (Purple Book; 1999). RIVM (2009) gives the value of delayed ignition as zero. RISCO (PTY) LTD believes the CPR 18E is more appropriate for warmer climates and is a conservative value.

4.4 Risk Criteria

4.4.1 Maximum Individual Risk Parameter

Standard individual risk parameters include: average individual risk; weighted individual risk; maximum individual risk; and, the fatal accident rate. The lattermost parameter is more applicable to occupational exposures.

Only the maximum individual risk (MIR) parameter will be used in this assessment. For this, parameter frequency of fatality is calculated for an individual who is presumed to be present at a specified location. This parameter (defined as the consequence of an event multiplied by the likelihood of the event) is not dependent on knowledge of populations at risk. So, it is an easier parameter to use in the predictive mode, than average individual risk or weighted individual risk. The unit of measure is the risk of fatality per person per year.

4.4.2 Acceptable Risks

The next step, after having characterised a risk and obtained a risk level, is to recommend whether the outcome is acceptable.

In contrast to the employees at a facility, who may be assumed to be healthy, the adopted exposure assessment applies to an average population group that also includes sensitive subpopulations. Sensitive subpopulation groups are those people that for reasons of age or medical condition have a greater than normal response to contaminants. Health guidelines and standards used to establish risk normally incorporate safety factors that address this group.

Among the most difficult tasks of risk characterisation is the definition of acceptable risk. In an attempt to account for risks in a manner similar to those used in everyday life, the UK Health and Safety Executive (HSE) developed the risk ALARP triangle. Applying the triangle involves deciding:

- Whether a risk is so high that something must be done about it;
- Whether the risk is or has been made so small that no further precautions are necessary;
- If a risk falls between these two states so that it has been reduced to levels as low as reasonably practicable (ALARP).

This is illustrated in Figure 4-1.

ALARP stands for 'as low as reasonably practicable'. As used in the UK, it is the region between that which is intolerable, at 1×10^{-4} per year, and that which is broadly acceptable, at 1×10^{-6} per year. A further lower level of risk, at 3×10^{-7} per year, is applied to either vulnerable or very large populations for land-use planning.

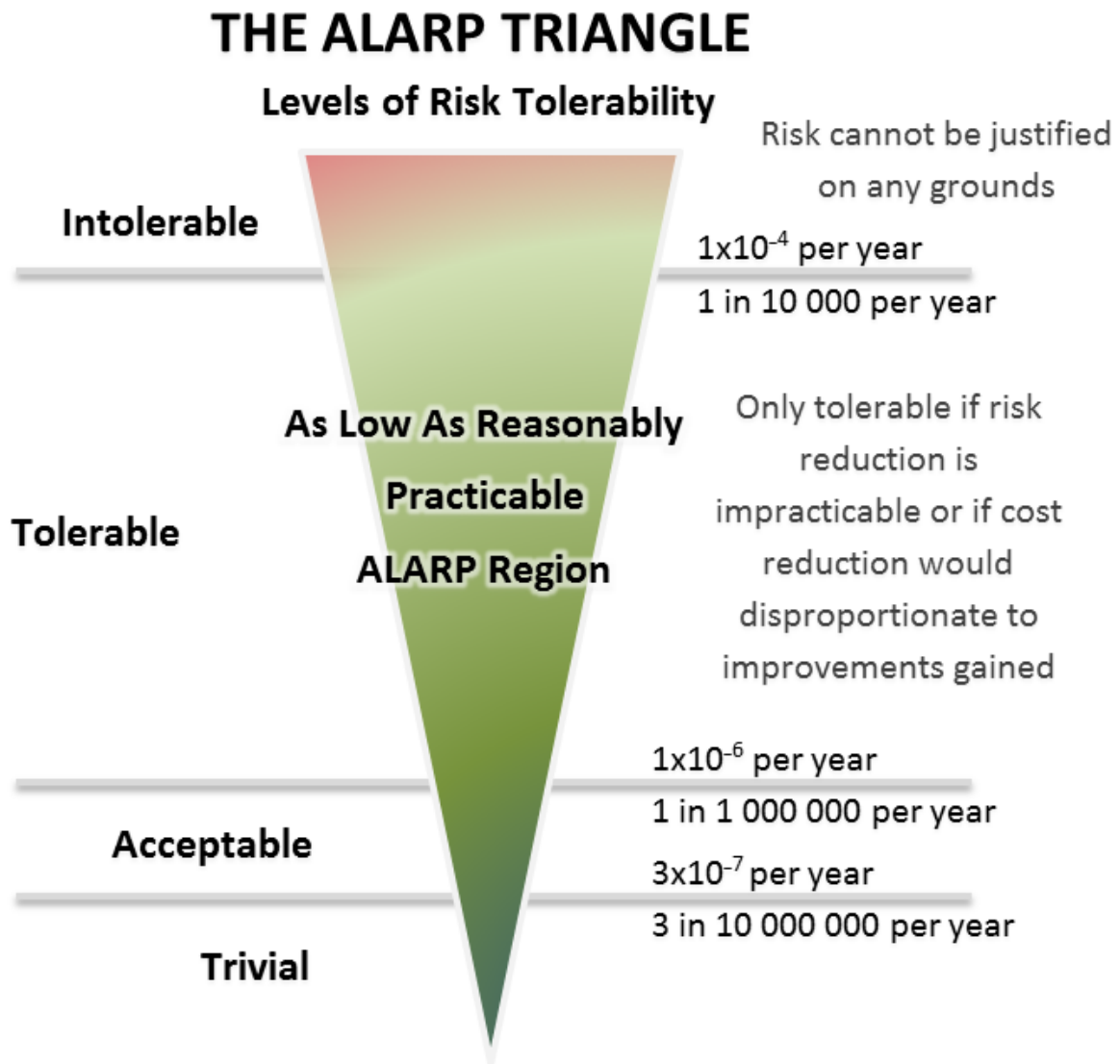


Figure 4-1: UK HSE decision-making framework

It should be emphasised that the risks considered acceptable to employees are different to those considered acceptable to the public. This is due to the fact that employees have personal protection equipment (PPE), are aware of the hazards, are sufficiently mobile to evade or escape the hazards and receive training in preventing injuries.

The HSE (UK) gives more detail on the word practicable in the following statement:

“ *In essence, making sure a risk has been reduced to ALARP is about weighing the risk against the sacrifice needed to further reduce it. The decision is weighted in favour of health and safety because the presumption is that the duty-holder should implement the risk reduction measure. To avoid having to make this sacrifice, the duty-holder must be able to show that it would be grossly disproportionate to the benefits of risk reduction that would be achieved. Thus, the process is not one of balancing the costs and benefits of measures but, rather, of adopting measures except where they are ruled out because they involve grossly disproportionate sacrifices. Extreme examples might be:*

- *To spend £1m to prevent five staff members suffering bruised knees is obviously grossly disproportionate; but,*
- *To spend £1m to prevent a major explosion capable of killing 150 people is obviously proportionate.*

Proving ALARP means that if the risks are lower than 1×10^{-4} fatalities per person per year, it can be demonstrated that there would be no more benefit from further mitigation, sometimes using cost benefit analysis. “

4.4.3 Land Planning

SANS 1461 (2018) provides guidelines for land planning criteria. This standard is a requirement for completing the MHI risk assessment. Thus, the land planning criteria can only be applied after completion of the MHI risk assessment, under Section 14 of the MHI regulation.

In this study, RISCOS can only suggest land planning approvals, based on the information provided and would require governmental authorities to make final decisions, based on the MHI risk assessment that would be completed after final designs.

Land zoning applied in this study follows the SANS 1461 (2018) and HSE (UK) approach of defining the area affected into three zones, consistent to the ALARP approach (HSE 2011).

The three zones are defined as follows:

- The inner zone is enclosed by the risk of 1×10^{-5} fatalities per person per year isopleth;
- The middle zone is enclosed by the risk of 1×10^{-5} fatalities per person per year and the risk of 1×10^{-6} fatalities per person per year isopleths;
- The outer zone is enclosed by the risk 1×10^{-6} fatalities per person per year and the risk of 3×10^{-7} fatalities per person per year isopleths.

The risks decrease from the inner zone to the outer zone, as shown in Figure 4-2 and Figure 4-3.

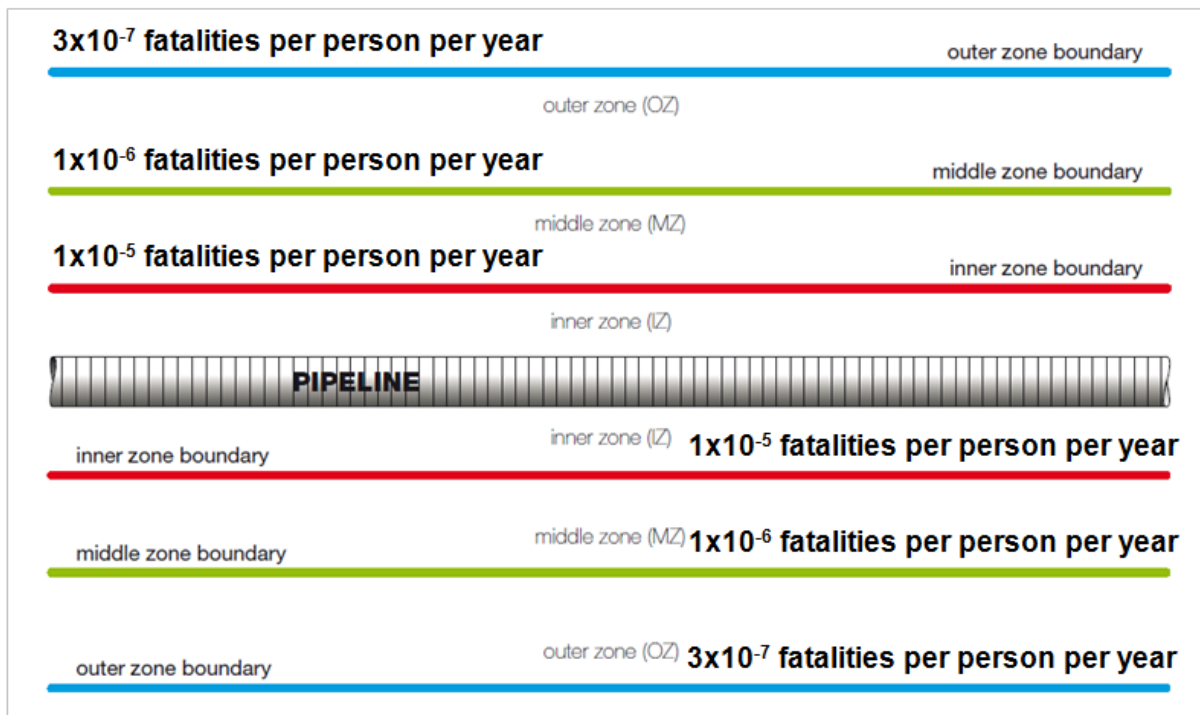


Figure 4-2: Town-planning zones for pipelines

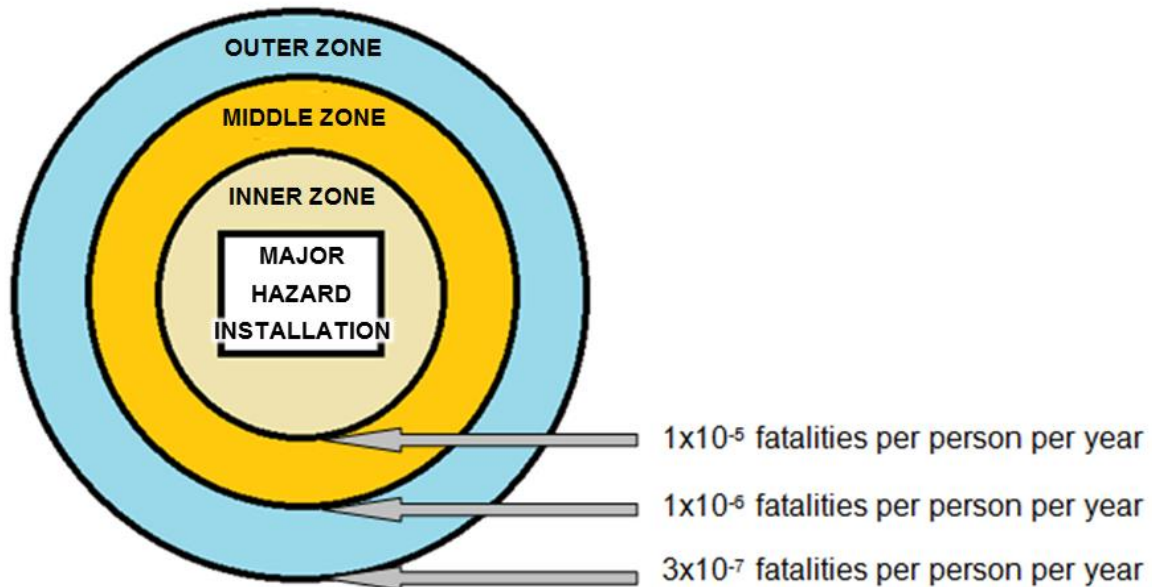


Figure 4-3: Town-planning zones

Once the zones are calculated, the HSE (UK) methodology then determines whether a development in a zone should be categorised as ‘advised against’ (AA) or as ‘don’t advise against’ (DAA), depending on the sensitivity of the development, as indicated in Table 4-17. There are no land-planning restrictions beyond the outer zone.

Table 4-17: Land-use decision matrix

Level of Sensitivity	Development in Inner Zone	Development in Middle Zone	Development in Outer Zone
1	DAA	DAA	DAA
2	AA	DAA	DAA
3	AA	AA	DAA
4	AA	AA	AA

The sensitivity levels are based on a clear rationale: progressively more severe restrictions are to be imposed as the sensitivity of the proposed development increases.

There are four sensitivity levels, with the sensitivity for housing defined as follows:

- Level 1 is based on workers who have been advised of the hazards and are trained accordingly;
- Level 2 is based on the general public at home and involved in normal activities;
- Level 3 is based on the vulnerability of certain members of the public (e.g., children, those with mobility difficulties or those unable to recognise physical danger);
- Level 4 is based on large examples of Level 2 and of Level 3.

Refer to Appendix B for detailed planning advice for developments near hazardous installations (PADHI) tables. These tables illustrate how the HSE land-use decision matrix, generated using the three zones and the four sensitivity levels, is applied to a variety of development types.

4.4.4 Societal Risk Parameter

Risk criteria discussed so far have been for individual risks. There is also a need to consider incidents in the light of their effect on many people at the same time. Public response to an incident that may harm many people is thought to be worse than the response to many incidents causing the same number of individual deaths. Compliance with an individual risk criterion is necessary but not always sufficient. Even if it were sufficient, societal risk would also have to be examined in some circumstances.

Societal risk is risk of widespread or large-scale harm from a potential hazard. The implication is that consequence would be on such a scale as to provoke a major social or political response and may lead to public discussion about regulation in general. Societal risk therefore takes into account, the density of the population around a Major Hazard Installation site and is the probability in any one year (F) of an event affecting at least a certain number (N) of people (also known as an FN curve).

4.4.5 Scenario Selection

The standard used for the calculation was SANS 1461 (2018), which describes that cross-country pipeline must be done to IGEM/TD/2 and PD 8010-3. Furthermore, the SANS 1461 (2018) is based on RIVM (2009). The respective event trees represented below were taken from the respective standards. The cross-country pipeline was underground with a vertical release, while the process piping and plant were above ground with a horizontal release.

4.4.5.1 Scenarios for Release of a Pressurised Liquefied Gas

The nature of the release of a liquefied gas from a pressurised vessel is dependent on the position of the hole.

A hole above the liquid level will result in a vapour release only, and the release rate would be related to the size of the hole and internal pressure of the tank. Over a period of time, bulk temperature reduces, with an associated decrease in the vapour release rate.

A hole below the liquid level will result in a release of a liquid stream. In the reduced pressure of the atmosphere, a portion of the liquid will vaporise at the normal boiling point. This phenomenon is called flashing and is shown in Figure 4-4. The pool, formed after flashing, then evaporates at a rate proportional to the pool area, surrounding temperature and wind velocity.

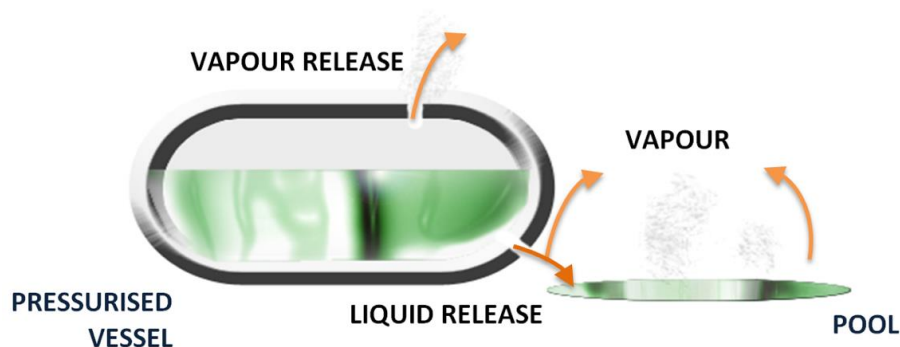


Figure 4-4: Airborne vapours from a loss of containment of liquefied gas stored in a pressurised vessel

4.4.5.2 Instantaneous Release of a Pressured Liquefied Flammable Gas

An instantaneous loss of containment of a liquefied flammable gas could result in the consequences given in the event tree of Figure 4-5. Probability of the events occurring is dependent on a number of factors and is determined accordingly. All the scenarios shown in the figure are determined separately and reported in relevant subsections of the report.

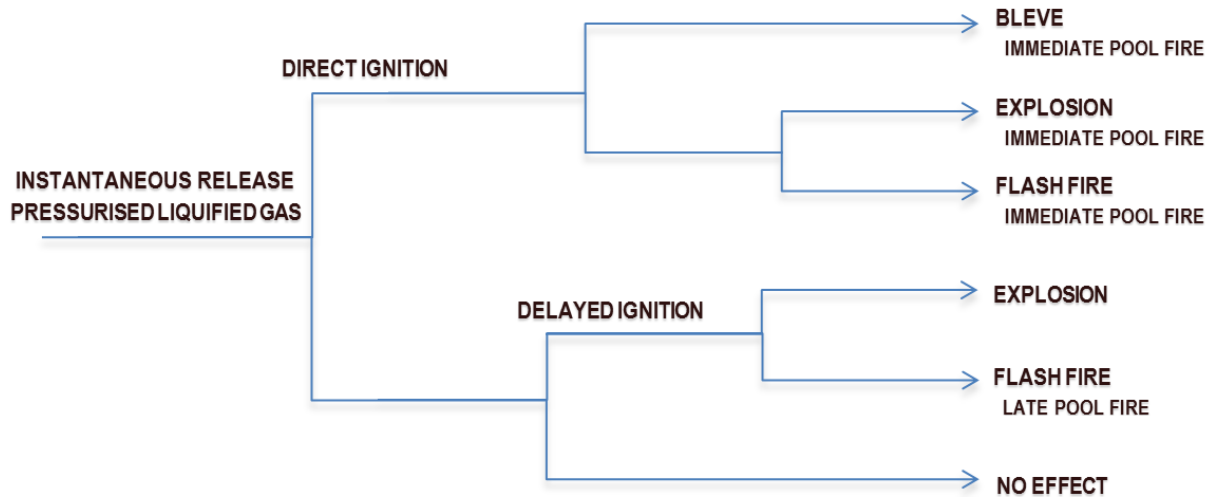


Figure 4-5: Event tree for an instantaneous release of a liquefied flammable gas

4.4.5.3 Continuous Release of a Pressurised Liquefied Flammable Gas

The continuous loss of containment of a liquefied flammable gas could result in the consequences given in the event tree of Figure 4-6. Probability of the events occurring is dependent on a number of factors and is determined accordingly. All the scenarios shown in the figure are determined separately and reported in relevant subsections of the report.

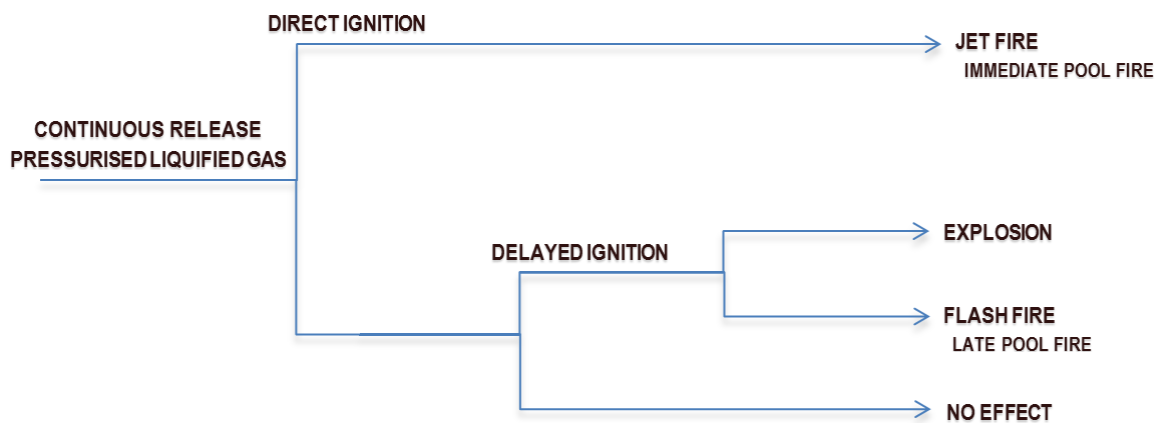


Figure 4-6: Event tree for a continuous release of a liquefied flammable gas

4.4.5.4 Continuous Release of a Flammable Gas

The continuous loss of containment of a flammable gas could result in the consequences given in the event tree of Figure 4-7. Probability of the events occurring is dependent on a number of factors and is determined accordingly. All the scenarios shown in the figure are determined separately and reported in relevant subsections of the report.

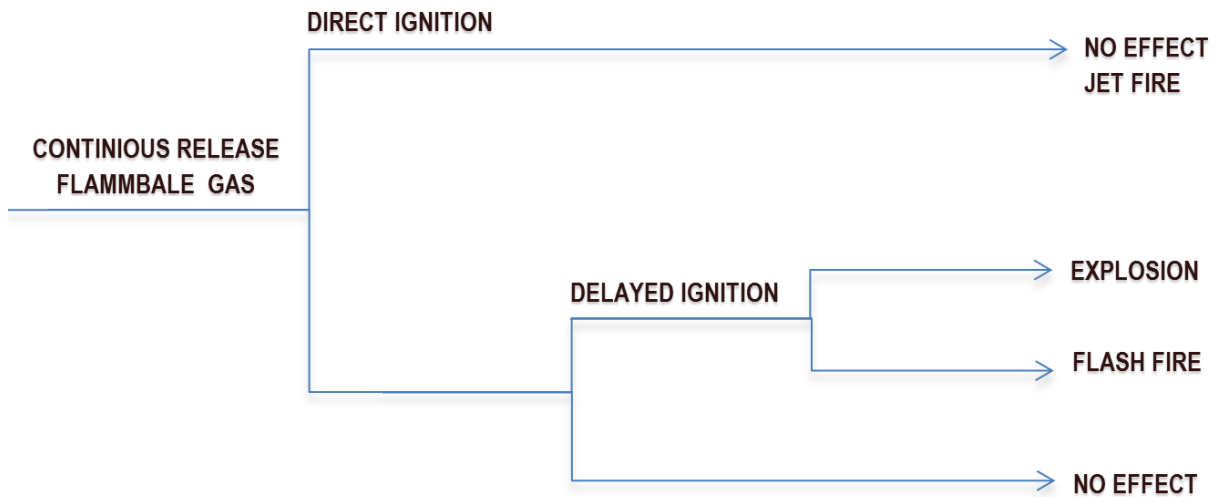


Figure 4-7: Event tree for a continuous release of a flammable gas

4.4.5.5 Continuous Release of a Flammable Liquid

The continuous loss of containment of a flammable liquid could result in the consequences given in the event tree of Figure 4-8. Probability of the events occurring is dependent on a number of factors and is determined accordingly. All the scenarios shown in the figure are determined separately and reported in relevant subsections of the report.

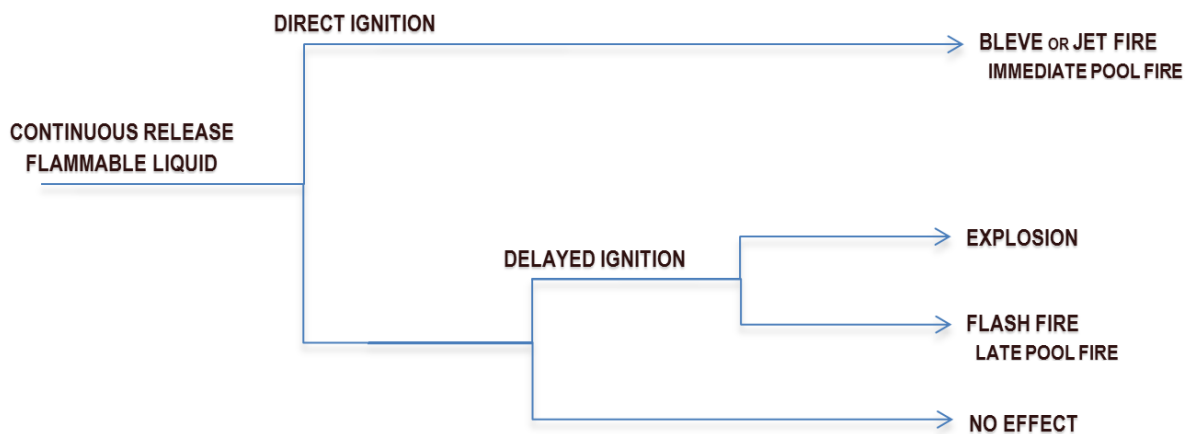


Figure 4-8: Event tree for a continuous release of a flammable liquid

5 RISK ASSESSMENT

Risk assessment was done of each processing unit by firstly selecting a scenario and then completing consequence and outflow modelling. Consequences with possible impacts beyond the site boundary were retained for risk analysis of the unit.

Finally, the risk of the entire facility is determined as a combination of the risk calculated for each unit.

5.1 Natural Gas Pipeline

5.1.1 The Purpose of the Processing Unit

The natural gas pipeline will tie into the main natural gas pipeline and end at the gas turbines. The process details at the incoming pipeline have not been established, nor the routing from the tie-in point to the gas turbines. For this study, the supply pressure was taken at 46 bar(g). The pipeline was assumed to be above ground with releases in the horizontal plane for the pipeline to the gas turbine. The supply pipeline was assumed to be below ground. The risk assessment of the underground pipeline leading up to the plant boundary was not part of the risk assessment.

5.1.2 Hazardous Components

Natural gas is a flammable substance with fire and explosion hazards, as described in Section 4.1.3.1.

5.1.3 Consequence Modelling

A loss of containment from a full-bore rupture could result in flash fires, vapour cloud explosions or jet fires. All of these scenarios are shown in Figure 5-1 to Figure 5-4, to the 1% fatality as a single loss of containment point. The thin solid lines (narrow plumes) indicate a release in a single direction, while the thick solid lines (concentric circles) indicate the extent from all wind directions. The orange line indicates the extent to the 1% fatality for the length of the pipeline to the gas turbine.

The scenario controlling the extent of the 1% fatality for the common supply and route option 1 and 2 is the Jet Fire and could extend beyond the site boundaries, impacting neighbours.

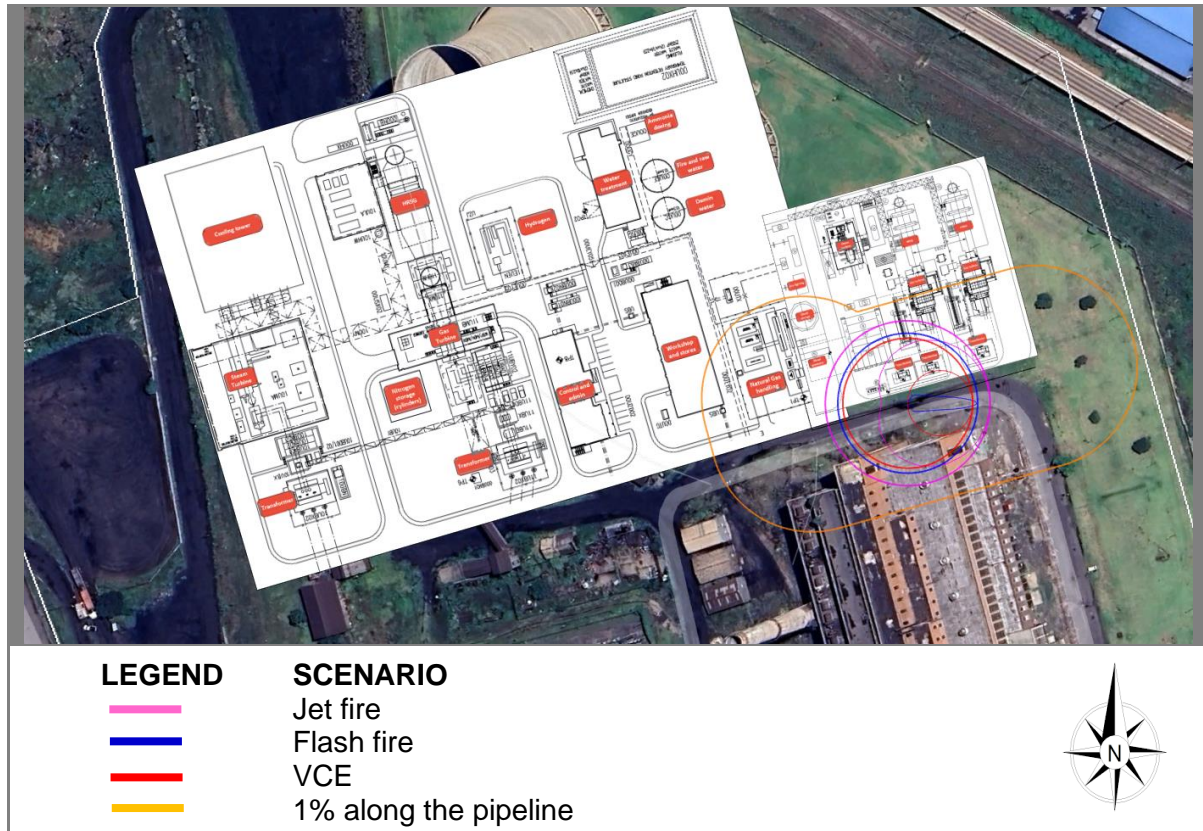


Figure 5-1: 1% Fatality along the pipeline routing of the common supply line

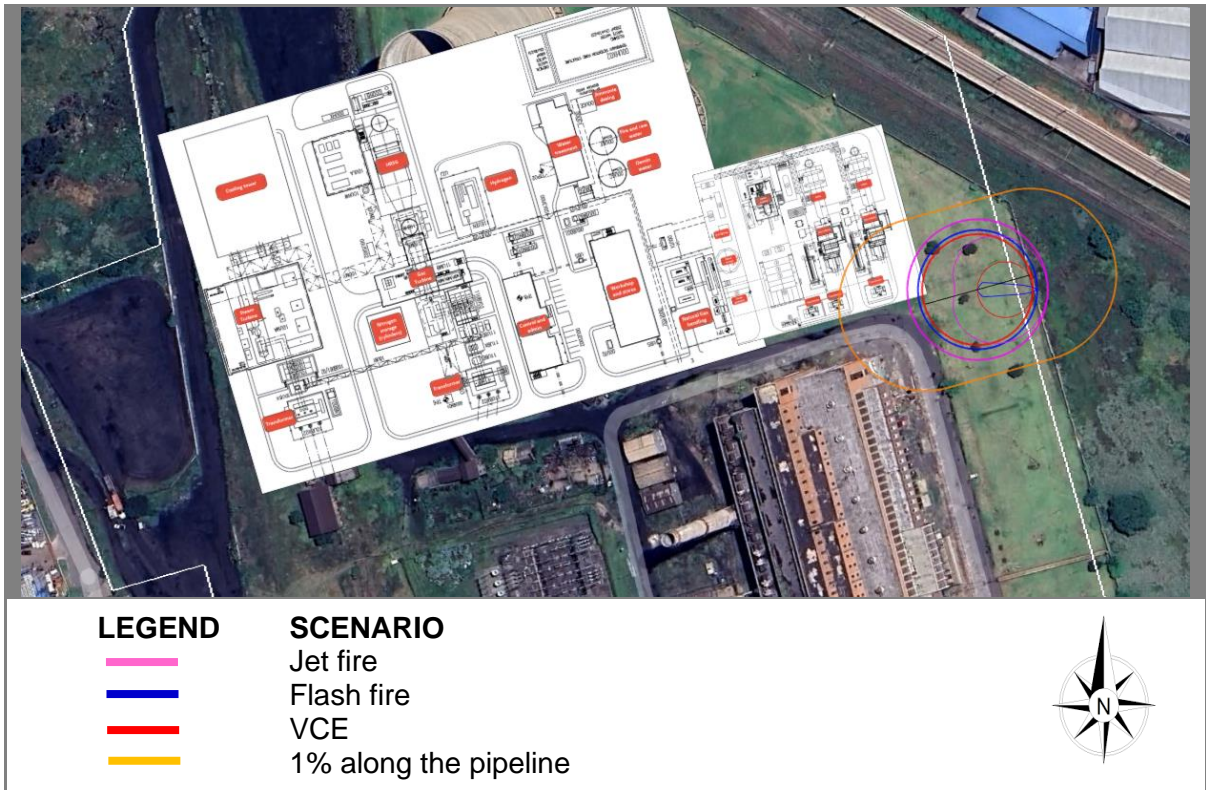


Figure 5-2: 1% Fatality along the pipeline routing of the supply route option 1

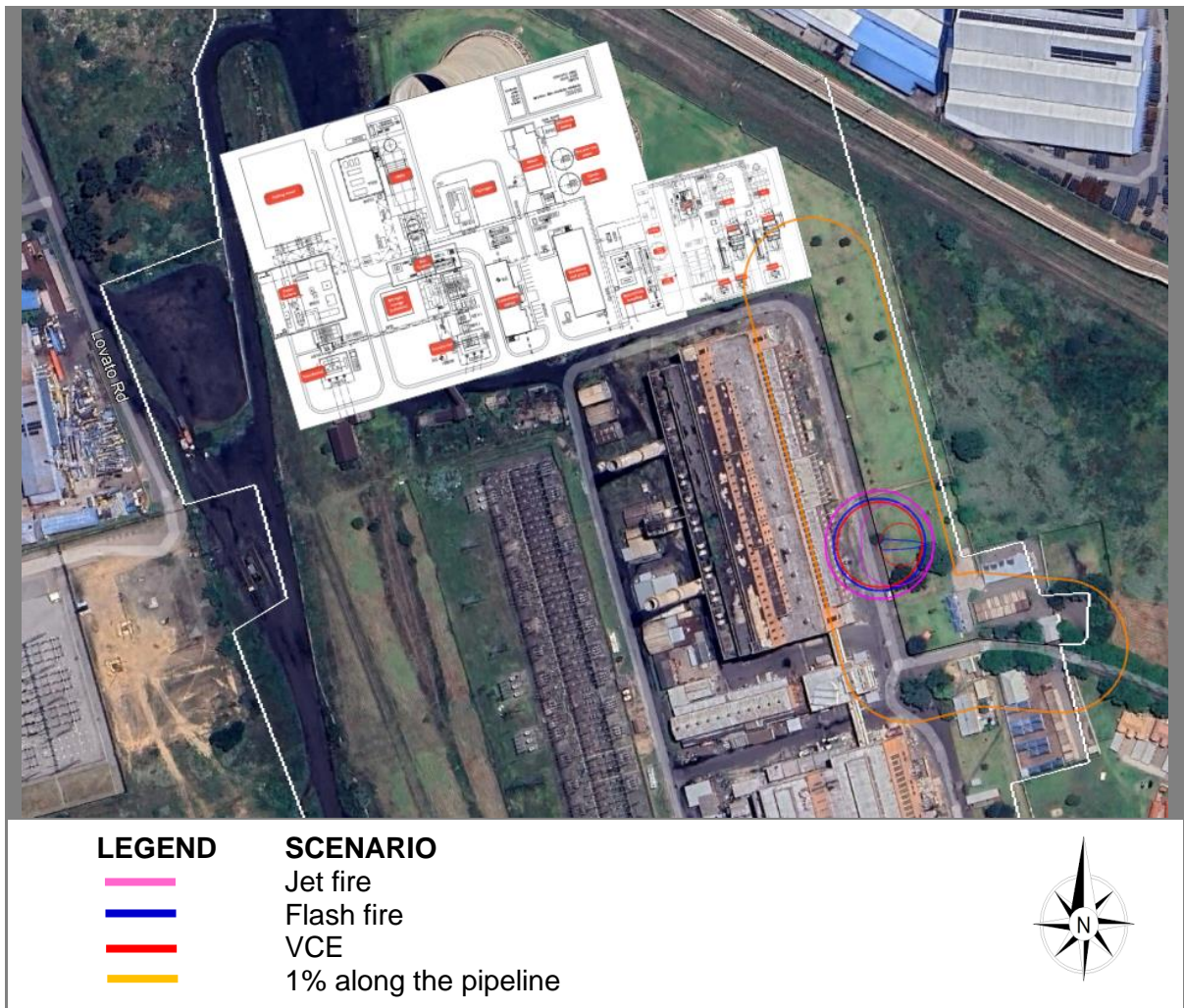


Figure 5-3: 1% Fatality along the pipeline routing of the supply route option 2

The scenario controlling the extent of the 1% fatality for the above ground pipeline to the gas turbine is the Flash Fire and could extend beyond the site boundaries, impacting neighbours.

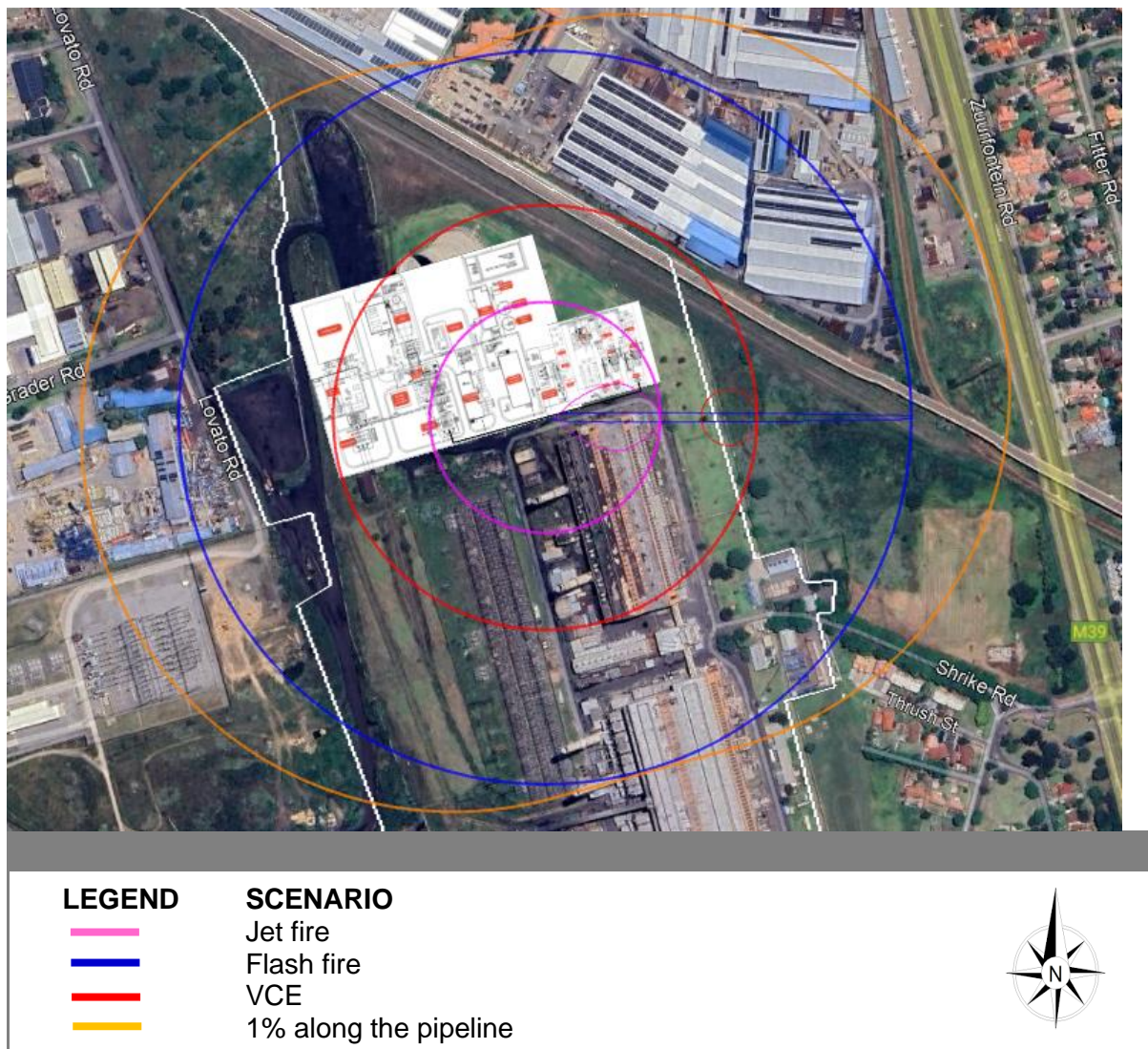


Figure 5-4: 1% Fatality along the pipeline routing to the gas turbine

5.2 Hydrogen Storage

5.2.1 The Purpose of the Processing Unit

Hydrogen will be delivered to site in hydrogen trailers. The trailer is assured to be that of a standard hydrogen trailer of 190 kg hydrogen inventory with a storage pressure at 226 bar(g).

5.2.2 Hazardous Components

Hydrogen is a flammable gas with fires and explosion potential and discussed in Section 4.1.3.1.

Most importantly, hydrogen produces an invisible flame.

5.2.3 Consequence Modelling

The scenarios modelled for the hydrogen trailer, are listed in Table 5-1.

Table 5-1: Scenarios modelled for the hydrogen trailer

Hydrogen trailer	<ul style="list-style-type: none"> • Catastrophic failure • 10 Minute release • 10 mm Hole 	<ul style="list-style-type: none"> • Jet fires • Flash fires. • Vapour cloud explosions • BLEVE
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5.2.4 Consequence Modelling

The loss of containment of hydrogen could result in fires and explosions. The maximum distance to the 1% fatality would be the catastrophic failure of the hydrogen trailer at a low wind speed.

The maximum extent to the 1% fatality from a catastrophic loss of containment, is shown in Figure 5-5. The thinner lines (narrow plumes) indicated the extent from a westerly wind, while the thicker lines (concentric circles) indicate the extent from all wind directions.

The extent of the 1% fatality could reach just beyond the site boundary, but would generally not impact surrounding communities.

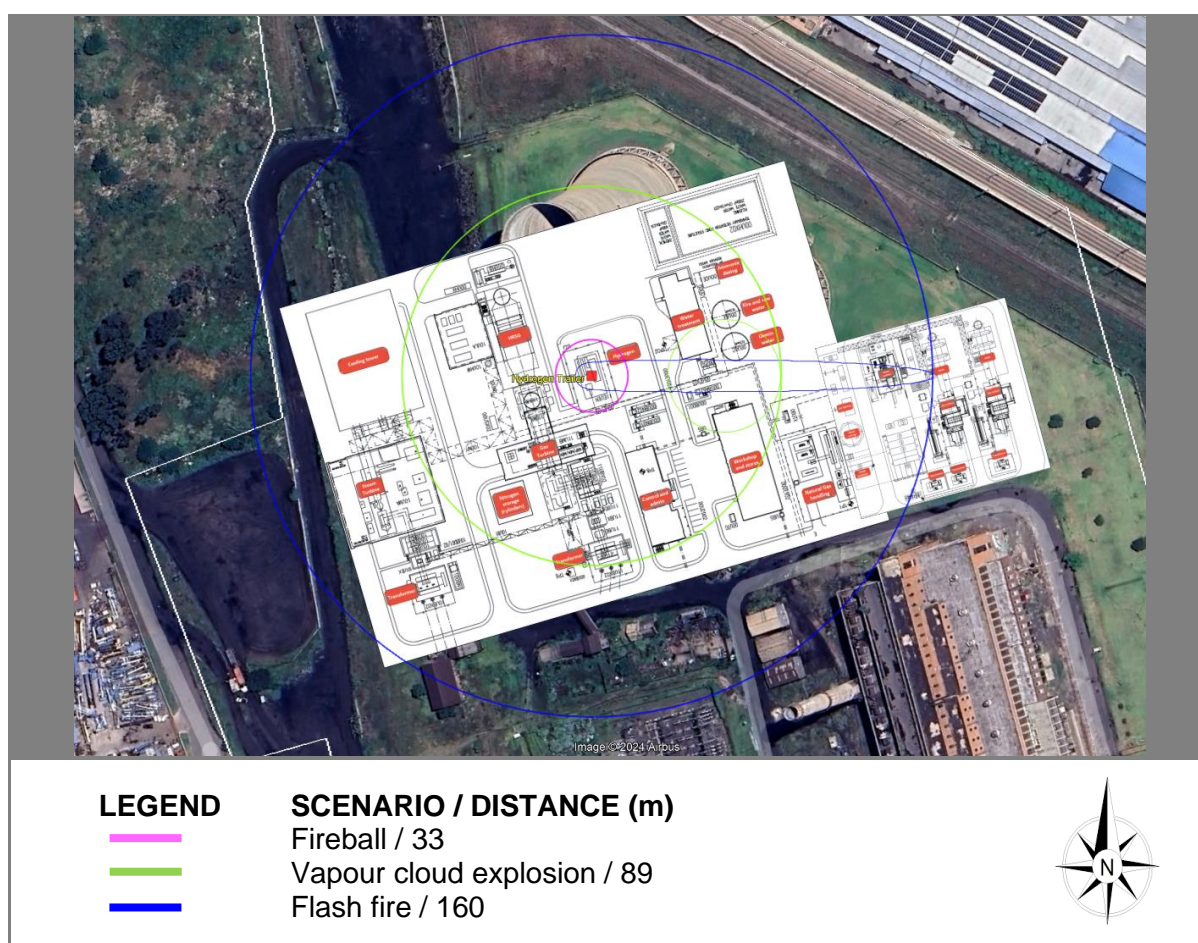


Figure 5-5: The extent to the 1% fatality from the worst-case loss of containment of the hydrogen trailer

5.3 Ammonia

Ammonia will be used to adjust the pH of the boiler water feed. The ammonia system has not been fully specified. For this study, ammonia was assumed to be stored in a 10 m³ cryogenic storage tank.

5.3.1 Hazardous Components

Ammonia is a highly toxic substance. The properties of ammonia are discussed in Section 4.1.3.1.

5.3.2 Consequence Modelling

The scenarios modelled for the ammonia storage, are listed in Table 5-2.

Table 5-2: Scenarios modelled for the ammonia transport pipeline and storage

Ammonia tank	<ul style="list-style-type: none"> • Catastrophic failure • 10 Minute release • 10 mm Hole 	Asphyxiation	<ul style="list-style-type: none"> • 10 m³ Cryogenic storage tank
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5.3.2.1 Toxic Vapour Clouds

Ammonia is a highly toxic component and could result in fatalities associated with a loss of containment.

Emergency Response Planning Guidelines (ERPGs) are airborne concentrations of chemicals that have been evaluated for three levels of emergency response. These are a nuisance level, and level that would affect egress from an exposure or a level that is near, but below a life-threatening concentration. ERPG-3 is the maximum air concentration below, which it is believed that nearly all individuals could be exposed without experiencing or developing life-threatening health effects. The ERPG-2 concentration is the maximum air concentration below, which it is believed nearly all individuals could be exposed without experiencing or developing irreversible or serious health effects or symptoms that could impair an individual's ability to take protective action. The ERPG-2 is used for emergency planning to indicate the furthest downwind distance to evacuation of nearby populations in the event of a release.

Figure 5-6 illustrates the ERPG-2 endpoint distances for various release scenarios in worst-case meteorological conditions. The ERPG-2 for the worst case (catastrophic failure) would extend 5 km downwind under a low wind speed condition (1.5 m.s^{-1}).

The thin lines (narrow plumes) indicate the shape of the plume from a westerly wind direction, while the thicker lines (concentric circles) indicate the extent of the plume from all directions. The westerly wind direction used does not indicate the predominant wind, but is used for illustrative purposes only.



Figure 5-6: The extent of the ERPG-2 values of ammonia following a large release, using the ERPG-2 value (150 ppm)

5.3.2.2 *Summary of Impacts*

Maximum distances from the point of release to the 1% fatality, are summarised for each scenario in Table 5-3.

Table 5-3: Maximum distance to 1% fatality from the point of release

Scenarios	Max. Distance to 1% Fatality (m)
Ammonia Tank	
Ammonia Tank - Catastrophic failure	258
Ammonia Tank - Fixed duration	392
Ammonia Tank -10 mm hole	199

5.5 Diesel Storage and Offloading

Diesel will be used for back-up generators. Diesel is considered combustible and will sustain combustion when lit. It is not considered toxic. The hazards of diesel are described in more detail in Section 4.1.3.1. For this study, diesel has not been assessed.

5.6 Nitrogen

Nitrogen will be used to purge flammable lines and equipment. The nitrogen system has not been fully specified. For this study, nitrogen has not been assessed.

6 RISK TREATMENT / REDUCTION

From the simulations performed, the areas of highest risk have been identified as the release of natural gas and ammonia.

Mitigations that may be considered, but not limited to reduce risks to acceptable levels are listed in the following subsections.

It should be noted that suggested mitigations are for consideration only. RISCUM does not imply that the suggested mitigation should be implemented or that any suggested mitigation is the only measure to reduce risks. Furthermore, implementation of some or all of the suggested mitigations would not guarantee full compliance with the Major Hazard Installation regulations.

Implementation of any mitigations should always be done in accordance with recognised engineering practices, using applicable codes and standards and be based on benefit versus cost principle.

6.1 Risk Ranking

This risk assessment considered numerous scenarios determining both consequences and a probability of release. Some scenarios have more serious consequences than others. However, the scenarios of particular interest are those with high-risk frequencies extending beyond the boundary of the site.

Figure 6-1 represents the 1×10^{-6} fatalities per person per year isopleth for the various site installations. The 1×10^{-6} fatalities per person per year isopleth is the lower limit for tolerable risks. The red curve represents the total site risk, while the other installations are shown in other colours. The major incidents would be from the natural gas pipeline.

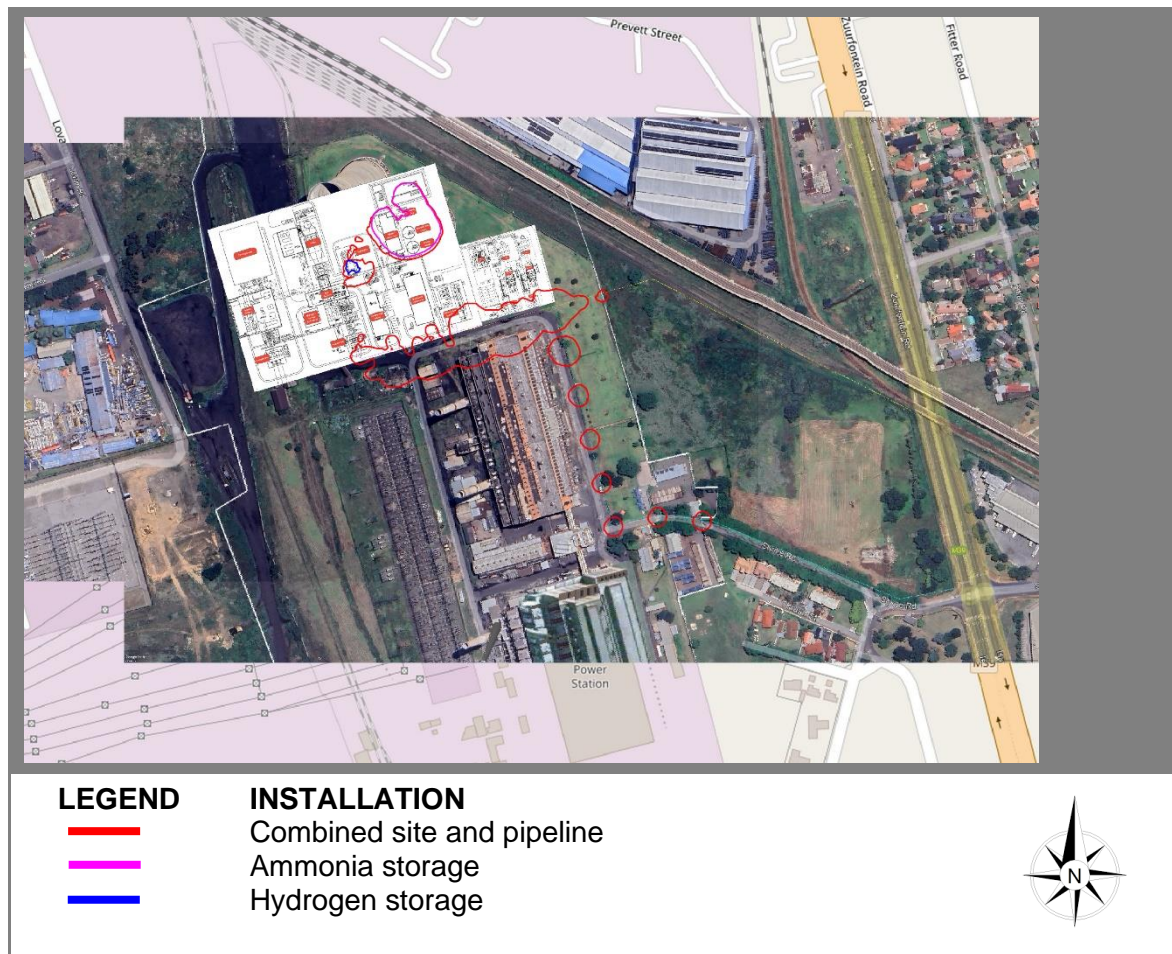


Figure 6-1: Comparison of the 1×10^{-6} fatalities per person per year isopleth for various site installations

6.2 Mitigation

As mentioned, the scenarios with the highest risk rankings are the natural gas pipeline operations. Suggested mitigation is listed in the following subsections.

6.2.1 Process Hazard Analysis (PHA)

Hazardous areas should be reviewed using detailed Process Hazard Analysis (PHA)¹ such as a HAZOP study that should be completed to identify potential hazards, and suggest further mitigation for safer operations.

6.2.2 Ignition Sources

Ignition sources near the depot must be minimised as far as possible. This is particularly relevant with the natural gas usage.

A hazardous area classification as per SANS 10108 must be developed for all flammable materials. Only suitable instrumentation and electrical equipment should be installed in accordance with the requirement of the code.

6.2.3 Emergency Shut Down System (ESD)

The fast detection of a loss of containment with appropriate shut-down action to limit the amount of natural gas released, will assist in the reduction of the site risks.

¹ A Process Hazard Analysis is not a regulated activity but merely identifies potential hazards and recommends mitigation

7 IMPACT ASSESSMENT

As described in the terms of reference of the project, assessment of the Impacts of the loss of containment scenarios considered in this study, took cognisance of the following aspects as they related to local population:

- An assessment of the magnitude of the impacts (the consequences of the project on members of the surrounding public);
- An assessment of the significance of the impacts, taking into account the sensitivity of the receptors;
- Development of mitigation measures to avoid, reduce or manage the impacts; and,
- Assessment of the residual significant impacts after applying the mitigation measures.

The criteria that were used in impact assessment are summarised below (verbatim from the terms of reference document):

For the purpose of this methodology the consequence of the impact is represented by:

$$C = \frac{(E + D + M + R) * N}{4}$$

- The **nature (N)**, which shall include a description of what causes the effect, what will be affected and how it will be affected.
- The **extent (E)**, wherein it will be indicated whether the impact will be local (limited to the immediate area or site of development) or regional, and a value between 1 and 5 will be assigned as appropriate (with 1 being low and 5 being high).
- The **duration (D)**, wherein it will be indicated whether:
 - the lifetime of the impact will be of a very short duration (0–1 years) – assigned a score of 1;
 - the lifetime of the impact will be of a short duration (1-5 years) - assigned a score of 2;
 - medium-term (6–15 years) – assigned a score of 3;
 - long term (the impact will cease after the operational life span of the project) - assigned a score of 4; or,
 - permanent - assigned a score of 5.
- The **magnitude (M)**, quantified on a scale from 1-5, where a score is assigned:
 - 1 is minor and will not result in an impact on processes;
 - 2 is low and will cause a slight impact on processes;
 - 3 is moderate and will result in processes continuing but in a modified way;
 - 4 is high (processes are altered to the extent that they temporarily cease);
 - 5 is very high and results in complete destruction of patterns and permanent cessation of processes.
- The **reversibility (R)**, quantified on a scale from 1-5, where a score is assigned:
 - 1 is impact is reversible without any time and cost;
 - 2 is impact is reversible without incurring significant time and cost;
 - 3 is impact is reversible only by incurring significant time and cost;
 - 4 is impact is reversible only by incurring prohibitively high time and cost;
 - 5 is impact is irreversible.

The result is a qualitative representation of relative ER associated with the impact. ER is therefore calculated as follows:

$$ER = C \times P$$

- The **probability of occurrence (P)**, which shall describe the likelihood of the impact actually occurring. Probability will be estimated on a scale of 1–5, where:
 - 1 is very improbable (probably will not happen);
 - 2 is low probability (some possibility, but low likelihood), 3 is medium probability (distinct possibility), 4 is high probability (most likely); and,
 - 5 is definite (impact will occur regardless of any prevention measures).

Table E-3: Determination of environmental risk

Consequence	5	5	10	15	20	25
	4	4	8	12	16	20
	3	3	6	9	12	15
	2	2	4	6	8	10
	1	1	2	3	4	5
		1	2	3	4	5
Probability						

The outcome of the environmental risk assessment will result in a range of scores, ranging from 1 through to 25. These ER scores are then grouped into respective classes as described in Table E-4.

Table E-4: Significance classes

Environmental Risk Score	
Value	Description
< 9	Low (i.e. where this impact is unlikely to be a significant environmental risk),
≥9; <17	Medium (i.e. where the impact could have a significant environmental risk),
≥ 17	High (i.e. where the impact will have a significant environmental risk).

7.1 Methodology - Cumulative Impacts

“Cumulative Impact”, in relation to an activity means the past, current and reasonably foreseeable future impact of an activity, considered together with the impact of activities associated with that activity, that in itself may not be significant, but may become significant when added to existing and reasonably foreseeable impacts eventuating from similar or diverse activities.

The role of the cumulative assessment is to test if such impacts are relevant to the proposed project in the proposed location (i.e., whether the addition of the proposed project in the area will increase the impact).

This section addresses whether the construction of the proposed development will result in:

- Unacceptable risk;
- Unacceptable loss;
- Complete or whole-scale changes to the environment or sense of place;
- Unacceptable increase in impact.

7.2 Impact Assessment of the proposed CCGT Thermal Generation Facility at Kempton Park

7.2.1 Natural Gas Pipeline

The following is the impact assessment of the natural gas installations:

Table 7-1: Impact Assessment of natural gas pipeline

Nature:		
Worst case loss of containment scenario – catastrophic rupture of natural gas pipeline leading to a fireball event, flammable vapour dispersion and ignition leading to flash fire thermal radiation effects and/or vapour cloud explosion overpressure effects.		
	Without Mitigation	With Mitigation
Extent	Site (2)	Activity (1)
Duration	Permanent (5)	Permanent (5)
Magnitude	Very high (5)	High (4)
Reversibility	Irreversible (worst case: death) (5)	Irreversible (worst case: death) (5)
Probability	Very improbable (1)	Very improbable (1)
Significance (environmental risk score)	Low (4)	Low (3)
Nature (positive or negative)	Negative	Negative
Irreplaceable loss of resources?	Yes (human)	Yes (human)
Can impacts be mitigated?	Yes	Yes
Mitigation:		
Mitigation would include emergency response arrangements and systems, such as alarms and shutdown systems to allow for personnel to muster in case of emergency, as well as fire-fighting systems and cooperation with emergency responders. Preventive measures would include maintenance procedures to prevent the occurrence of a catastrophic loss of containment from corrosion, fire and gas detection and firewater systems to prevent escalation as well as strict control of ignition sources and other measures, which may be required according to standards such as those prescribed by the South African National Standards system.		
Residual Risks:		
Even with mitigation, there may be residual risk of occurrence due to failures in protection systems and break-down in procedures and documented systems.		

7.2.3 Hydrogen Installation

The following is the impact assessment of the hydrogen storage installations:

Table 7-2: Impact Assessment of Hydrogen Storage Installations

Nature:		
Worst case loss of containment scenario – catastrophic rupture of hydrogen storage vessel leading to leading to a fireball event, flammable vapour dispersion and ignition leading to flash fire thermal radiation effects and/or vapour cloud explosion overpressure effects.		
	Without Mitigation	With Mitigation
Extent	Site (2)	Activity (1)
Duration	Permanent (5)	Permanent (5)
Magnitude	High (4)	High (4)
Reversibility	Irreversible (worst case: death) (5)	Irreversible (worst case: death) (5)
Probability	Very improbable (1)	Very improbable (1)
Significance (environmental risk score)	Low (3)	Low (3)
Status (positive or negative)	Negative	Negative
Irreplaceable loss of resources?	Yes (human)	Yes (human)
Can impacts be mitigated?	Yes	Yes
Mitigation:		
Mitigation would include emergency response arrangements and systems, such as alarms to allow for personnel to muster in case of emergency, as well as fire-fighting systems and cooperation with emergency responders. Preventive measures would include maintenance procedures to prevent the occurrence of a catastrophic loss of containment from corrosion, fire and gas detection and firewater systems to prevent escalation, as well as strict control of ignition sources and other measures, which may be required according to standards such as those prescribed by the South African National Standards system.		
Residual Risks:		
Even with mitigation, there may be residual risk of occurrence due to failures in protection systems and break-down in procedures and documented systems.		

7.2.4 Ammonia Storage

The following is the impact assessment of the Ammonia installations:

Table 7-3: Impact Assessment of ammonia storage

Nature:		
Worst case loss of containment of ammonia scenario – leading to a release of toxic airborne plumes.		
	Without Mitigation	With Mitigation
Extent	Site (2)	Activity (1)
Duration	Permanent (5)	Permanent (5)
Magnitude	Very high (5)	High (4)
Reversibility	Irreversible (worst case: death) (5)	Irreversible (worst case: death) (5)
Probability	Very improbable (1)	Very improbable (1)
Significance (environmental risk score)	Low (4)	Low (3)
Status (positive or negative)	Negative	Negative
Irreplaceable loss of resources?	Yes (human)	Yes (human)
Can impacts be mitigated?	Yes	Yes
Mitigation:		
Mitigation would include reduction of ammonia or substitution for a less toxic component emergency response arrangements and systems, such as alarms to allow for personnel to muster in case of emergency, and cooperation with emergency responders. Preventive measures would include design, installation according to the vendor requirements. Furthermore, the layout separation distances between battery storage units and other units to prevent knock-on effects.		
Residual Risks:		
Even with mitigation, there may be residual risk of occurrence due to failures in protection systems and break-down in procedures and documented systems.		

7.2.5 Cumulative Impact Assessment

This section considers all impacts in the preceding Section 7.2 and the cumulative impact of all installations.

The risks of the site are dominated by the natural gas pipeline, and thus the cumulative impact will be identical to the natural gas pipeline.

Table 7-4: Cumulative impact of project as a whole

Nature:		
Worst case loss of containment scenario – catastrophic rupture of natural gas pipeline leading to a fireball event, flammable vapour dispersion and ignition leading to flash fire thermal radiation effects and/or vapour cloud explosion overpressure effects.		
	Without Mitigation	With Mitigation
Extent	Site (2)	Activity (1)
Duration	Permanent (5)	Permanent (5)
Magnitude	Very high (5)	High (4)
Reversibility	Irreversible (worst case: death) (5)	Irreversible (worst case: death) (5)
Probability	Very improbable (1)	Very improbable (1)
Significance (environmental risk score)	Low (4)	Low (12)
Status (positive or negative)	Negative	Negative
Irreplaceable loss of resources?	Yes (human)	Yes (human)
Can impacts be mitigated?	Yes	Yes
Mitigation:		
Mitigation would include emergency response arrangements and systems, such as alarms and shutdown systems to allow for personnel to muster in case of emergency, as well as fire-fighting systems and cooperation with emergency responders. Preventive measures would include maintenance procedures to prevent the occurrence of a catastrophic loss of containment from corrosion, fire and gas detection and firewater systems to prevent escalation as well as strict control of ignition sources and other measures, which may be required according to standards such as those prescribed by the South African National Standards system.		
Residual Risks:		
Even with mitigation, there may be residual risk of occurrence due to failures in protection systems and break-down in procedures and documented systems.		

8 CONCLUSIONS

Risk calculations are not precise. Accuracy of predictions is determined by the quality of base data and expert judgements.

This risk assessment included the consequences of fires and explosions at the proposed CCGT facility in Kempton Park. A number of well-known sources of incident data were consulted and applied to determine the likelihood of an incident to occur.

This risk assessment was performed with the assumption that the site would be maintained to an acceptable level and that all statutory regulations would be applied. It was also assumed that the detailed engineering designs would be done by competent people, and would be correctly specified for the intended duty. For example, it was assumed that tank wall thicknesses have been correctly calculated, that vents have been sized for emergency conditions, that instrumentation and electrical components comply with the specified electrical area classification, that material of construction is compatible with the products, etc.

It is the responsibility of the owners and their contractors to ensure that all engineering designs would have been completed by competent persons, and that all pieces of equipment would have been installed correctly. All designs should be in full compliance with (but not limited to) the Occupational Health and Safety Act 85 of 1993 and its regulations, the National Buildings Regulations and the Buildings Standards Act 107 of 1977 as well as local bylaws.

A number of incident scenarios were simulated, taking into account the prevailing meteorological conditions, and described in the report.

8.1 Notifiable Substances

The General Machinery Regulation 8 and its Schedule A on notifiable substances, requires any employer who has a substance equal to or exceeding the quantity listed in the regulation to notify the divisional director. A site is classified as a Major Hazard Installation if it contains one or more notifiable substances, or if the off-site risk is sufficiently high. The latter can only be determined from a quantitative risk assessment.

The notifiable threshold for ammonia is listed as 20 tonne in a single vessel. As the proposed installation should not exceed the threshold limit, ammonia will not be classified as a notifiable substance.

8.2 Power Plant and Associated Equipment

Hazardous substances associated with this facility would include; ammonia; hydrogen, diesel and natural gas. Of the listed substances, only ammonia and natural gas could result in offsite fatalities.

The risk of 1×10^{-6} fatalities per person per year isopleth found to be immediately beyond but primarily within the site boundary.

8.3 Impacts onto Neighbouring Properties, Residential Areas and Major Hazard Installations

A large release of ammonia could extend a considerable downward distance impacting the commercial and residential areas of Kempton Park, Edenvale and Lethabong. However, fatalities will be limited to the industrial area and will not impact residential areas.

No residential area or vulnerable institutions would be seriously impacted with the construction and operation of the proposed CCGT.

8.4 Major Hazard Installation

This investigation concluded that under the current design conditions, the proposed CCGT facility in Kempton Park **would be considered as a Major Hazard Installation** and would require notification in accordance with the MHI regulations.

According to chapter 3 the “Classification of pipelines as major hazard establishment” of Major Hazard Installation Regulations, 2022:

A pipeline is considered an establishment if it contains a fluid which is or is to be conveyed in a pipeline as a gas which is flammable in air (is applicable to flammable gases conveyed as a gas. In such cases the additional duties only apply when the flammable gas is conveyed at a pressure in excess of 8 bars absolute. This covers such fluids as methane, butane and propane).

Kindly note that this study is not intended to replace the Major Hazard Installation risk assessment, which should be completed prior to construction of the terminal once final designs are available.

8.5 Land Planning Restrictions

The risks generated from this study concluded that the risk isopleths generated from the proposed project could have risks within the ALARP range, resulting in land planning restrictions. As the designs have not been finalised, the full land planning restrictions must be taken from the Major Hazard Installation risk assessment report.

9 RECOMMENDATIONS

As a result of the risk assessment study conducted for the proposed CCGT facility in Kempton Park, a number of events were found to have risks beyond the site boundary. These risks could be mitigated to acceptable levels, as shown in the report.

RISCOM did not find any fatal flaws that would prevent the project proceeding to the detailed engineering phase of the project, and would support the project under the following conditions most of which will be detailed in the MHI study:

- Compliance with all statutory requirements, i.e., pressure vessel designs;
- Compliance with applicable SANS codes, i.e., SANS 10087, SANS 10089, SANS 10108, etc. ;
- Incorporation of applicable guidelines or equivalent international recognised codes of good design and practice into the designs;
- Completion of a recognised process hazard analysis (such as a HAZOP study, FMEA, etc.) on the proposed facility prior to construction to ensure design and operational hazards have been identified and adequate mitigation put in place;
- Full compliance with IEC 61508 and IEC 61511 (Safety Instrument Systems) standards or equivalent to ensure that adequate protective instrumentation is included in the design and would remain valid for the full life cycle of the tank farm:
 - Including demonstration from the designer that sufficient and reliable instrumentation would be specified and installed at the facility;
- Preparation and issue of a safety document detailing safety and design features reducing the impacts from fires, explosions and flammable atmospheres to the MHI assessment body at the time of the MHI assessment:
 - Including compliance to statutory laws, applicable codes and standards and world's best practice;
 - Including the listing of statutory and non-statutory inspections, giving frequency of inspections;
 - Including the auditing of the built facility against the safety document;
 - Noting that codes such as IEC 61511 can be used to achieve these requirements;
- Demonstration by the CCGT owner or their contractor that the final designs would reduce the risks posed by the installation to the South African requirements as prescribed in SANS 1461 (2018);
- Signature of all terminal designs by a professional engineer registered in South Africa in accordance with the Professional Engineers Act, who takes responsibility for suitable designs;
- Completion of an emergency preparedness and response document for on-site and off-site scenarios prior to initiating the MHI risk assessment (with input from local authorities);
- Any increases to the product list or product inventories must be with the approval of the authorities under NEMA;
- Final acceptance of the facility risks with an MHI risk assessment that must be completed in accordance with the MHI regulations;
 - Basing such a risk assessment on the final design and including engineering mitigation.

10 REFERENCES

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11 ABBREVIATIONS AND ACRONYMS

AIA	See Approved Inspection Authority
ALARP	<p>The UK Health and Safety Executive (HSE) developed the risk ALARP triangle, in an attempt to account for risks in a manner similar to those used in everyday life. This involved deciding:</p> <ul style="list-style-type: none"> • Whether a risk is so high that something must be done about it; • Whether the risk is or has been made so small that no further precautions are necessary; • Whether a risk falls between these two states and has been reduced to levels 'as low as reasonably practicable' (ALARP). <p>Reasonable practicability involves weighing a risk against the trouble, time and money needed to control it.</p>
API	The American Petroleum Institute is the largest U.S. trade association for the oil and natural gas industry. It claims to represent nearly 600 corporations involved in production, refinement, distribution, and many other aspects of the petroleum industry.
Approved Inspection Authority	An approved inspection authority (AIA) is defined in the Major Hazard Installation regulations (July 2001)
Asphyxiant	An asphyxiant is a gas that is nontoxic but may be fatal if it accumulates in a confined space and is breathed at high concentrations since it replaces oxygen containing air.
Blast Overpressure	Blast overpressure is a measure used in the multi-energy method to indicate the strength of the blast, indicated by a number ranging from 1 (for very low strengths) up to 10 (for detonative strength).
BLEVE	Boiling liquid expanding vapour explosions result from the sudden failure of a vessel containing liquid at a temperature above its boiling point. A BLEVE of flammables results in a large fireball.
CCGT	A closed-cycle gas turbine is a turbine that uses a gas (e.g., air, nitrogen, helium, argon, etc.) for the working fluid as part of a closed thermodynamic system. Heat is supplied from an external source. Such recirculating turbines follow the Brayton cycle.
Detonation	Detonation is a release of energy caused by extremely rapid chemical reaction of a substance, in which the reaction front of a substance is determined by compression beyond the auto-ignition temperature.
EIA	Environmental assessment is the assessment of the environmental consequences of a plan, policy, program, or actual projects prior to the decision to move forward with the proposed action.
Emergency Plan	An emergency plan is a plan in writing that describes how potential incidents identified at the installation together with their consequences should be dealt with, both on site and off site.
ERPG	<p>Emergency response planning guidelines were developed by the American Industrial Hygiene Association.</p> <p>ERPG-1 is the maximum airborne concentration below which it is believed nearly all individuals could be exposed for up to 1 hour without experiencing anything other than mild transient adverse health effects or perceiving a clearly defined objectionable odour.</p> <p>ERPG-2 is the maximum airborne concentration below which it is believed nearly all individuals could be exposed for up to 1 hour without</p>

	<p>experiencing or developing irreversible or other serious health effects or symptoms that could impair their abilities to take protective action.</p> <p>ERPG-3 is the maximum airborne concentration below which it is believed nearly all individuals could be exposed for up to 1 hour without experiencing or developing life-threatening health effects.</p>
ESD	Emergency Shutdown System (ESD) is designed to minimize the consequences of emergency situations, related to typically uncontrolled flooding, escape of hydrocarbons, or outbreak of fire in hydrocarbon carrying areas or areas which may otherwise be hazardous.
Explosion	An explosion is a release of energy that causes a pressure discontinuity or blast wave.
Flammable Limits	Flammable limits are a range of gas or vapour concentrations in the air that will burn or explode if a flame or other ignition source is present. The lower point of the range is called the lower flammable limit (LFL). Likewise, the upper point of the range is called the upper flammable limit (UFL).
Flammable Liquid	<p>The Occupational Health and Safety Act 85 of 1993 defines a flammable liquid as any liquid which produces a vapour that forms an explosive mixture with air and includes any liquid with a closed cup flashpoint of less than 55°C.</p> <p>Flammable products have been classified according to their flashpoints and boiling points, which ultimately determine the propensity to ignite. Separation distances described in the various codes are dependent on the flammability classification.</p> <p>Class Description</p> <p>0 Liquefied petroleum gas (LPG)</p> <p>IA Liquids that have a closed cup flashpoint of below 23°C and a boiling point below 35°C</p> <p>IB Liquids that have a closed cup flashpoint of below 23°C and a boiling point of 35°C or above</p> <p>IC Liquids that have a closed cup flashpoint of 23°C and above but below 38°C</p> <p>II Liquids that have a closed cup flashpoint of 38°C and above but below 60.5°C</p> <p>IIA Liquids that have a closed cup flashpoint of 60.5°C and above but below 93°C</p>
Flash Fire	A flash fire is defined as combustion of a flammable vapour and air mixture in which the flame passes through the mixture at a rate less than sonic velocity so that negligible damaging overpressure is generated.
FMEA	Failure mode and effects analysis is the process of reviewing as many components, assemblies, and subsystems as possible to identify potential failure modes in a system and their causes and effects
Frequency	Frequency is the number of times an outcome is expected to occur in a given period of time.
HAZOP	A hazard and operability study (HAZOP) are a structured and systematic examination of a complex planned or existing process or operation in order to identify and evaluate problems that may represent risks to personnel or equipment.
HEL	The maximum concentration of a gas or vapor that will burn in air is defined as the Upper Explosive Limit (UEL) . Above this level, the

	mixture is too “rich” to burn. The range between the LEL and UEL is known as the flammable range for that gas or vapor.
HRSG	A heat recovery steam generator is a kind of heat exchanger that recovers heat from the exhaust gases of a gas turbine to an extreme degree. The heat is recovered in the form of steam which is served as the power source of a power-generating steam turbine.
HV	High voltage electricity refers to electrical potential large enough to cause injury or damage. In certain industries, high voltage refers to voltage above a certain threshold. Equipment and conductors that carry high voltage warrant special safety requirements and procedures.
Ignition Source	An ignition source is a source of temperature and energy sufficient to initiate combustion.
Individual Risk	Individual risk is the probability that in one year a person will become a victim of an accident if the person remains permanently and unprotected in a certain location. Often the probability of occurrence in one year is replaced by the frequency of occurrence per year.
Isopleth	See Risk Isopleth
Jet	A jet is the outflow of material emerging from an orifice with significant momentum.
Jet Fire or Flame	A jet fire or flame is combusting material emerging from an orifice with a significant momentum.
LEL	Lower Explosive Limit is defined as the lowest concentration (by percentage) of a gas or vapor in air that is capable of producing a flash of fire in presence of an ignition source (arc, flame, heat). ... In concentrations of 0-5% Methane in air, the mixture is too lean to ignite or burn.
LFL	Lower Flammable Limit see Flammable Limits
LPG	Liquefied natural gas (LPG) is natural gas (predominantly methane, CH ₄ , with some mixture of ethane, C ₂ H ₆) that has been cooled down to liquid form for ease and safety of non-pressurized storage or transport.
LOC	See Loss of Containment
Local Government	Local government is defined in Section 1 of the Local Government Transition Act, 1993 (Act No. 209 of 1993).
Loss of Containment	Loss of containment (LOC) is the event resulting in a release of material into the atmosphere.
Major Hazard Installation	Major Hazard Installation (MHI) means an installation: <ul style="list-style-type: none"> • Where more than the prescribed quantity of any substance is or may be kept, whether permanently or temporarily; • Where any substance is produced, used, handled or stored in such a form and quantity that it has the potential to cause a major incident (the potential of which will be determined by the risk assessment).
Major Incident	A major incident is an occurrence of catastrophic proportions, resulting from the use of plant or machinery or from activities at a workplace. When the outcome of a risk assessment indicates that there is a possibility that the public will be involved in an incident, then the incident is catastrophic.
Material Safety Data Sheet	According to ISO-11014, a material safety data sheet (MSDS) is a document that contains information on the potential health effects of exposure to chemicals or other potentially dangerous substances and on safe working procedures when handling chemical products. It is an essential starting point for the development of a complete health and

	safety program. It contains hazard evaluations on the use, storage, handling and emergency procedures related to that material. An MSDS contains much more information about the material than the label and it is prepared by the supplier. It is intended to tell what the hazards of the product are, how to use the product safely, what to expect if the recommendations are not followed, what to do if accidents occur, how to recognize symptoms of overexposure and what to do if such incidents occur.
MHI	See Major Hazard Installation
MIR	Maximum Individual Risk (see Individual Risk)
MSDS	See Material Safety Data Sheet
NEMA	National Environmental Management Act 107 of 1998, abbreviated (NEMA) is the statutory framework to enforce Section 24 of the Constitution of the Republic of South Africa. The NEMA is intended to promote co-operative governance and ensure that the rights of people are upheld, but also recognising the necessity of economic development.
OHS Act	Occupational Health and Safety Act, 1993 (Act No. 85 of 1993)
PAC	See Protective Action Criteria
PADHI	<p>PADHI (planning advice for developments near hazardous installations) is the name given to a methodology and software decision support tool developed and used in the HSE. It is used to give land-use planning (LUP) advice on proposed developments near hazardous installations.</p> <p>PADHI uses two inputs into a decision matrix to generate either an 'advise against' or 'don't advise against' response:</p> <ul style="list-style-type: none"> The zone in which the development is located of the three zones that HSE sets around the major hazard: <ul style="list-style-type: none"> The inner zone ($> 1 \times 10^{-5}$ fatalities per person per year); The middle zone (1×10^{-5} fatalities per person per year to 1×10^{-6} fatalities per person per year); The outer zone (1×10^{-6} fatalities per person per year to 3×10^{-7} fatalities per person per year); The 'sensitivity level' of the proposed development which is derived from an HSE categorisation system of 'development types' (see the 'development type tables' in Appendix B).
PHA	A process hazard analysis is a set of organized and systematic assessments of the potential hazards associated with an industrial process.
POST	The Parliamentary Office of Science and Technology is the Parliament of the United Kingdom's in-house source of independent, balanced and accessible analysis of public policy issues related to science and technology.
PPM	This is an abbreviation for " parts per million " and it also can be expressed as milligrams per liter (mg/L). This measurement is the mass of a chemical or contaminate per unit volume of water.
QRA	See Quantitative Risk Assessment
Quantitative Risk Assessment	A quantitative risk assessment is the process of hazard identification, followed by a numerical evaluation of effects of incidents, both consequences and probabilities and their combination into the overall measure of risk.

Risk	Risk is the measure of the consequence of a hazard and the frequency at which it is likely to occur. Risk is expressed mathematically as: Risk = Consequence x Frequency of Occurrence
Risk Assessment	Risk assessment is the process of collecting, organising, analysing, interpreting, communicating and implementing information in order to identify the probable frequency, magnitude and nature of any major incident which could occur at a major hazard installation and the measures required to remove, reduce or control potential causes of such an incident.
Risk Contour	See Risk Isopleth
SANAS	The South African National Accreditation System (SANAS) is the only national body responsible for carrying out accreditations in respect of conformity assessment, as mandated through the Accreditation for Conformity Assessment, Calibration and Good Laboratory Practice Act (Act 19 of 2006).
Societal Risk	Societal risk is risk posed on a societal group who are exposed to a hazardous activity.
UFL	Upper Flammable Limit (see Flammable Limits)
Vapour Cloud Explosion	A vapour cloud explosion (VCE) results from ignition of a premixed cloud of a flammable vapour, gas or spray with air, in which flames accelerate to sufficiently high velocities to produce significant overpressure.
VCE	See Vapour Cloud Explosion

12 APPENDIX A: NOTIFICATION OF MAJOR HAZARD INSTALLATION

Prior to assessment of potential impacts of various accidental spills, reference needs to be made to the legislation, regulations and guidelines governing the operation of the development.

Section 1 of the Occupational Health and Safety Act (OHS Act; Act No. 85 of 1993) defines a "major hazard installation" to mean an installation:

- “
- (a) *Where more than the prescribed quantity of any substance is or may be kept, whether permanently or temporarily;*
 - (b) *Where any substance is produced, processed, used, handled or stored in such a form and quantity that it has the potential to cause a major incident (our emphasis).*
- “

It should be noted that if either (a) or (b) is satisfied, the Major Hazard Installation (MHI) regulations will apply. The prescribed quantity of a chemical can be found in Section 8 (1) of the General Machinery Regulation 8 (our emphasis).

A major incident is defined as: "an occurrence of catastrophic proportions, resulting from the use of plant and machinery or from activities at a workplace". Catastrophic in this context means loss of life and limbs or severe injury to employees or members of the public, particularly those who are in the immediate vicinity (our emphasis).

It is important to note that the definition refers to an occurrence, whereas Section 1b) refers to potential to cause a major incident. If potential to cause a major incident exists, then the OHS Act and the Major Hazard Installation regulations will apply (our emphasis).

On the 16th of January 1998, the MHI regulations were promulgated under the OHS Act (Act No. 85 of 1993), with a further amendment on the 31st of January 2023. The provisions of the regulations apply to installations that have on their premises a certain quantity of a substance that can pose a significant risk to the health and safety of employees and the public.

The scope of application given in Regulation 2 of the MHI regulations is as follows:

- “
- (1) *These Regulations apply to–*
 - (a) *major hazard installations;*
 - (b) *establishments with the prescribed quantity of substances listed in Chapter 1 or 2; and*
 - (c) *major pipeline establishments.*
 - (2) *These Regulations, excluding regulations 11, 12 and 13, apply to low hazard establishments.*
 - (3) *These Regulations, excluding regulations 12 and 13, apply to medium hazard establishments.*
 - (4) *Regulations 14 and 15 apply to local government.*
 - (5) *Regulations 21 and 22 apply to an approved inspection authority.*
 - (6) *These Regulations do not apply to nuclear installations registered in terms of the Nuclear Energy Act, 1993 (Act No. 131 of 1993).*
- “

It is important to note that the regulations refer to a substance, and furthermore the regulations are applicable to risks posed by the substance and **NOT** merely the potential consequences (our emphasis).

The regulations essentially consist of various parts, namely:

1. The duties for notification and registration of a MHI (regulation 4 and 5);
2. The minimum requirements for a QRA (regulation 10);
3. Major incident prevention policy (regulation 11);
4. Safety report (regulation 12);
5. Licence to operate (section 13);
6. The general duties required of local government (regulation 14);
7. The requirements for an on-site emergency plan (regulation 15);
8. The reporting steps for risk and emergency occurrences (regulation 16);
9. Information and training (regulation 17);
10. The general duties required of suppliers (regulation 18);
11. The duties of approved inspection authority (regulation 22).

Notification of installation (regulation 4) indicates that:

- A duty holder must notify the chief inspector, the relevant chief director: provincial operations and the local government on Form A, 90 days–
 - To erect any Major Hazard Installation;
 - when there is an anticipated change to an existing establishment.
- A duty holder, after the entry into force of these Regulations, must update the notification of an existing establishment and send it to the chief inspector, the relevant chief director: provincial operations and the local government on a prescribed form A, within 24 months.
- The notification must be accompanied by–
 - proof of permission or approval from the relevant local government on land use indicating the exact location of the site;
 - a letter of designation and the responsible person's competency profile;
 - an inventory list and safety data sheets of all the dangerous substances that resulted in the installation being classified as an establishment;
 - a statement containing the envisaged maximum quantity of all the substances that may be present at the establishment at any one time;
 - the most recent risk assessment report contemplated in regulation 10;
 - a site map showing the establishment location and indicating developments around the vicinity of the establishment;
 - a substance location plan drawn to a scale of not less than 1 to 2 500 which identifies the area on the site where the dangerous substances will be stored, handled, used or processed, showing the location of the major items of plant used in such activities;
 - information regarding the neighbours or other establishments within the impact zone;
 - proof of the publication of the advertisement; and
 - where applicable, the latest version of the major incident prevention policy.

The risk assessment (regulation 10):

- A duty holder must, after consultation with the relevant health and safety representative or health and safety committee, ensure that an approved inspection authority carries out a risk assessment in accordance with SANS 1461 at intervals not exceeding five years or when there is a change in the establishment.
- Every duty holder must—
 - inform the relevant health and safety representative or health and safety committee, in writing, of the arrangements made to carry out a risk assessment contemplated in subregulation (1); and
 - ensure that the results of the risk assessment are made available to the relevant health and safety representative or committee, who may comment thereon.
- Where a risk assessment has been reviewed or revised, without a change to the establishment, the duty holder must submit an updated copy of the risk assessment report to the chief inspector, the relevant chief director: provincial operations and the relevant local government within 60 days.
- Every duty holder must ensure that a copy of the most recent risk assessment report is available on site for inspection by an inspector or a local government.
- Subregulation (1) shall not apply in the case of rolling stock in transit: Provided that the operator of a railway shall ensure—
 - that a risk assessment applicable to rolling stock in transit is carried out and made available for inspection at the request of an inspector or a local government or both that inspector and that local government, as the case may be; and
 - that, in the interest of the health and safety of the public, the necessary precautions are taken.
- A duty holder shall ensure that the risk assessments contemplated in subregulations (1) and (3) be made available for scrutiny by any affected or interested person that may be affected by the activities of the establishment, at a time and place and in a manner agreed upon between the parties.

Requirements related to the on-site emergency plan (regulation 15) are:

- A duty holder must, immediately after submission of the notification contemplated in regulation 4, in consultation with the relevant health and safety representatives or health and safety committee, in writing, appoint an emergency coordinating team consisting of at least—
 - the responsible person contemplated in regulation 3(2); or
 - a responsible person's deputy contemplated in regulation 3(3); and
 - a representative from the health and safety committee.
- The duty holder must develop and maintain an on-site emergency plan before the establishment commences operations in consultation with the emergency coordinating team and in accordance with SANS 1514.
- The on-site emergency plan for an existing establishment must be aligned and updated to SANS 1514 within 12 months after the entry into force of these Regulations.
- A duty holder must—
 - ensure that the manner in which employees, visitors and neighbours will be warned of major incidents is included in the plan;
 - sign a copy of the on-site emergency plan in the presence of at least two witnesses who have knowledge in emergency planning and who must be satisfied with the content of the emergency plan and attest to the signature of the duty holder;
 - obtain approval of the on-site emergency plan from the relevant local government;
 - ensure that the on-site emergency plan is readily available at all times for implementation and use;
 - cause the on-site emergency plan to be tested or exercised in practice at least once a year and take the necessary steps to arrange for the local government to participate in such tests; and
 - give an early warning to affected or interested parties in case a major incident is likely to go beyond the borders of the establishment.
- The duty holder and the relevant local government must take reasonable steps to activate the on-site emergency plan in case of an incident which may result in—
 - a major incident; or
 - an uncontrolled event which may reasonably be expected to lead to a major incident; or
 - a near miss that could reasonably be expected to have resulted in a major incident.
- The duty holder must review the on-site emergency plan at least once every three years and, if necessary, revise the plan.
- The duty holder and the local government must jointly ensure that all first responders at the scene of a major incident have the necessary skill to deal with the dangerous substances and are dressed in the appropriate emergency personal protective equipment as required in their respective emergency plans.

The general duties of local government (regulation 14) are summarised as follows:

- Without derogating from the provisions of the National Building Regulations and Building Standards Act, 1977 (Act No. 103 of 1977), and the Spatial Planning and Land Use Management Act, 2013 (Act No. 16 of 2013), a local government must not permit the erection of a new establishment or the expansion of an establishment at a separation distance that poses an unacceptable risk in terms of the risk assessment contemplated in regulation 10.
- The local government must—
 - permit a new development only where there is a separation distance which will not pose an unacceptable risk in terms of the risk assessment contemplated in regulation 10; and
 - prohibit any new property development adjacent to an establishment that will result in that new development being declared an establishment.
- The relevant local government must give consent for the on-site emergency plan and participate in the annual emergency test drill as contemplated in regulation 15(4)(e).
- Where a relevant local government does not have the facilities available to control a major incident or to comply with the requirements of these Regulations, that local government must make prior arrangements with a neighbouring local government, the relevant provincial government or the duty holder for assistance.
- The relevant local government is responsible for the off-site emergency plan to be followed outside the premises of the establishment.
- The relevant local government must prepare an off-site emergency plan in accordance with SANS 1514 and in consultation with the duty holder and interested or affected persons, within 24 months after the entry into force of these Regulations, and thereafter immediately for new establishments, and review the plan when there are significant changes to the hazard profile of the area.
- The duty holder must, on written request by, and within the time limits imposed by the local government, furnish the local government with the necessary information needed to prepare the off-site emergency plan.

In reporting of risk and emergency occurrences (regulation 16):

- A duty holder must—
 - Subject to the provisions of Regulation 8 of the General Administrative Regulations, within 48 hours by means of telephone, facsimile or similar means of communication, inform the chief inspector of the occurrence of a major incident or an incident that brought the emergency plan into operation or any near miss;
 - Investigate and submit a written preliminary incident report to the chief inspector within seven days after an emergency occurrence and a major incident;
 - Submit a final report as soon as reasonably practicable but not later than six months after the incident
 - Investigate and record all near misses in a register kept on the premises, which shall at all times be available for inspection by an inspector and local government representatives.
- A duty holder must, in the case of an emerging major incident or an emergency occurrence that was or may have been caused by a dangerous substance, inform the supplier of that dangerous substance about the incident.

The general duties of the supplier (regulation 18) refer specifically to:

- Every person that supplies a dangerous substance to an establishment must issue a safety data sheet that is supplied with the substance and must also provide basic information for training on the use and handling of the substance.
- A supplier of a dangerous substance involved in an emerging major incident or potential major incident must inform all clients supplied with that substance of the emerging potential dangers surrounding the dangerous substance.
- A supplier must, in the event of a major incident with regard to the dangerous substance supplied, provide information and advice that must be readily available on a 24-hour basis to all duty holders, the relevant local government and any other body concerned.

13 APPENDIX B: PADHI LAND-PLANNING TABLES

13.1 Development Type Table 1: People at Work, Parking

Development Type	Examples	Development Detail and Size	Justification
DT1.1 Workplaces	Offices, factories, warehouses, haulage depots, farm buildings, nonretail markets, builder's yards	Workplaces (predominantly nonretail), providing for less than 100 occupants in each building and less than 3 occupied storeys (Level 1)	Places where the occupants will be fit and healthy and could be organised easily for emergency action Members of the public will not be present or will be present in very small numbers and for a short time
	Exclusions		
		DT1.1 x1 Workplaces (predominantly nonretail) providing for 100 or more occupants in any building or 3 or more occupied storeys in height (Level 2 except where the development is at the major hazard site itself, where it remains Level 1)	Substantial increase in numbers at risk with no direct benefit from exposure to the risk
	Sheltered workshops, Remploy	DT1.1 x2 Workplaces (predominantly nonretail) specifically for people with disabilities (Level 3)	Those at risk may be especially vulnerable to injury from hazardous events or they may not be able to be organised easily for emergency action
DT1.2 Parking Areas	Car parks, truck parks, lockup garages	Parking areas with no other associated facilities (other than toilets; Level 1)	
	Exclusions		
	Car parks with picnic areas or at a retail or leisure development or serving a park and ride interchange	DT1.2 x1 Where parking areas are associated with other facilities and developments the sensitivity level and the decision will be based on the facility or development	

13.2 Development Type Table 2: Developments for Use by the General Public

Development Type	Examples	Development Detail and Size	Justification
DT2.1 Housing	Houses, flats, retirement flats or bungalows, residential caravans, mobile homes	Developments up to and including 30 dwelling units and at a density of no more than 40 per hectare (Level 2)	Development where people live or are temporarily resident It may be difficult to organise people in the event of an emergency
	Exclusions		
	Infill, back-land development	DT2.1 x1 Developments of 1 or 2 dwelling units (Level 1)	Minimal increase in numbers at risk
	Larger housing developments	DT2.1 x2 Larger developments for more than 30 dwelling units (Level 3)	Substantial increase in numbers at risk
		DT2.1 x3 Any developments (for more than 2 dwelling units) at a density of more than 40 dwelling units per hectare (Level 3)	High-density developments
DT2.2 Hotel or Hostel or Holiday Accommodation	Hotels, motels, guest houses, hostels, youth hostels, holiday camps, holiday homes, halls of residence, dormitories, accommodation centres, holiday caravan sites, camping sites	Accommodation up to 100 beds or 33 caravan or tent pitches (Level 2)	Development where people are temporarily resident It may be difficult to organise people in the event of an emergency
	Exclusions		
	Smaller: guest houses, hostels, youth hostels, holiday homes, halls of residence, dormitories, holiday caravan sites, camping sites	DT2.2 x1 Accommodation of less than 10 beds or 3 caravan or tent pitches (Level 1)	Minimal increase in numbers at risk
	Larger: hotels, motels, hostels, youth hostels, holiday camps, holiday homes, halls of residence, dormitories, holiday caravan sites, camping sites	DT2.2 x2 Accommodation of more than 100 beds or 33 caravan or tent pitches (Level 3)	Substantial increase in numbers at risk

Development Type	Examples	Development Detail and Size	Justification
DT2.3 Transport Links	Motorway, dual carriageway	Major transport links in their own right i.e., not as an integral part of other developments (Level 2)	Prime purpose is as a transport link Potentially large numbers exposed to risk but exposure of an individual is only for a short period
	Exclusions		
	Estate roads, access roads	DT2.3 x1 Single carriageway roads (Level 1)	Minimal numbers present and mostly a small period of time exposed to risk Associated with other development
	Any railway or tram track	DT2.3 x2 Railways (Level 1)	Transient population, small period of time exposed to risk Periods of time with no population present

Development Type	Examples	Development Detail and Size	Justification
DT2.4 Indoor Use by Public	Food and drink: restaurants, cafes, drive-through fast food, pubs Retail: shops, petrol filling station (total floor space based on shop area not forecourt), vehicle dealers (total floor space based on showroom or sales building not outside display areas), retail warehouses, super-stores, small shopping centres, markets, financial and professional services to the public Community and adult education: libraries, art galleries, museums, exhibition halls, day surgeries, health centres, religious buildings, community centres. adult education, 6th form college, college of FE Assembly and leisure: Coach or bus or railway stations, ferry terminals, airports, cinemas, concert or bingo or dance halls, conference centres, sports or leisure centres, sports halls, facilities associated with golf courses, flying clubs (e.g., changing rooms, club house), indoor go kart tracks	Developments for use by the general public where total floor space is from 250 m ² up to 5000 m ² (Level 2)	Developments where members of the public will be present (but not resident) Emergency action may be difficult to coordinate
	Exclusions		
		DT2.4 x1 Development with less than 250 m ² total floor space (Level 1)	Minimal increase in numbers at risk
		DT2.4 x2 Development with more than 5000 m ² total floor space (Level 3)	Substantial increase in numbers at risk
DT2.5 Outdoor Use by Public	Food and drink: food festivals, picnic areas Retail: outdoor markets, car boot sales, funfairs	Principally an outdoor development for use by the general public i.e., developments	Developments where members of the public will be present (but

Development Type	Examples	Development Detail and Size	Justification
	Community and adult education: open-air theatres and exhibitions Assembly and leisure: coach or bus or railway stations, park and ride interchange, ferry terminals, sports stadia, sports fields or pitches, funfairs, theme parks, viewing stands, marinas, playing fields, children's play areas, BMX or go kart tracks, country parks, nature reserves, picnic sites, marquees	where people will predominantly be outdoors and not more than 100 people will gather at the facility at any one time (Level 2)	not resident) either indoors or outdoors Emergency action may be difficult to coordinate
	Exclusions		
	Outdoor markets, car boot sales, funfairs picnic area, park and ride interchange, viewing stands, marquees	DT2.5 x1 Predominantly open-air developments likely to attract the general public in numbers greater than 100 people but up to 1000 at any one time (Level 3)	Substantial increase in numbers at risk and more vulnerable due to being outside
	Theme parks, funfairs, large sports stadia and events, open air markets, outdoor concerts, pop festivals	DT2.5 x2 Predominantly open-air developments likely to attract the general public in numbers greater than 1000 people at any one time (Level 4)	Very substantial increase in numbers at risk, more vulnerable due to being outside Emergency action may be difficult to coordinate

13.3 Development Type Table 3: Developments for Use by Vulnerable People

Development Type	Examples	Development Detail and Size	Justification
DT3.1 Institutional Accommodation and Education	Hospitals, convalescent homes, nursing homes, old people's homes with warden on site or 'on call', sheltered housing, nurseries, crèches, schools and academies for children up to school leaving age	Institutional, educational and special accommodation for vulnerable people or that provides a protective environment (Level 3)	Places providing an element of care or protection Because of age, infirmity or state of health the occupants may be especially vulnerable to injury from hazardous events Emergency action and evacuation may be very difficult
	Exclusions		
	Hospitals, convalescent homes, nursing homes, old people's homes, sheltered housing	DT3.1 x1 24-hour care where the site on the planning application being developed is larger than 0.25 hectare (Level 4)	Substantial increase in numbers of vulnerable people at risk
	Schools, nurseries, crèches	DT3.1 x2 Day care where the site on the planning application being developed is larger than 1.4 hectare (Level 4)	Substantial increase in numbers of vulnerable people at risk
DT3.2 Prisons	Prisons, remand centres	Secure accommodation for those sentenced by court, or awaiting trial, etc. (Level 3)	Places providing detention Emergency action and evacuation may be very difficult

13.4 Development Type Table 4: Very Large and Sensitive Developments

Development Type	Examples	Development Detail and Size	Justification
Note: all Level 4 developments are by exception from Level 2 or 3 and are reproduced in this table for convenient reference			
DT4.1 Institutional Accommodation	Hospitals, convalescent homes, nursing homes, old people's homes, sheltered housing	Large developments of institutional and special accommodation for vulnerable people (or that provide a protective environment) where 24-hour care is provided and where the site on the planning application being developed is larger than 0.25 hectare (Level 4)	Places providing an element of care or protection Because of age or state of health the occupants may be especially vulnerable to injury from hazardous events Emergency action and evacuation may be very difficult The risk to an individual may be small but there is a larger societal concern
	Nurseries, crèches, schools for children up to school leaving age	Large developments of institutional and special accommodation for vulnerable people (or that provide a protective environment) where day care (not 24-hour care) is provided and where the site on the planning application being developed is larger than 1.4 hectare (Level 4)	Places providing an element of care or protection Because of the occupants that may be especially vulnerable to injury from hazardous events Emergency action and evacuation may be very difficult The risk to an individual may be small but there is a larger societal concern
DT4.2 Very Large Outdoor Use by Public	Theme parks, large sports stadia and events, open air markets, outdoor concerts, pop festivals	Predominantly open-air developments where there could be more than 1000 people present (Level 4)	People in the open air may be more exposed to toxic fumes and thermal radiation than if they were in buildings Large numbers make emergency action and evacuation difficult The risk to an individual may be small but there is a larger societal concern

14 APPENDIX C: DEPARTMENT OF EMPLOYMENT AND LABOUR
CERTIFICATE



employment & labour

Department:
Employment and Labour
REPUBLIC OF SOUTH AFRICA

National Department of Employment and Labour
Republic of South Africa

APPROVED INSPECTION AUTHORITY

*Registered in accordance with the provisions of the Occupational Health and Safety Act,
Act 85 of 1993, as amended and the Major Hazard Installation Regulations.*

THIS IS TO CERTIFY THAT:

RISCOM (PTY) LTD

*has been registered by the Department of Employment and Labour as an Approved Inspection
Authority: Type A, to conduct Major Hazard Installation Risk Assessment, in terms of Regulation
5(5)(a), of the Major Hazard Installation Regulations.*

CONDITIONS OF REGISTRATION:

- The AIA must at all time comply with the requirements of the Occupational Health and Safety Act, Act 85 of 1993, as amended.
- This registration certificate is not transferable.
- This registration will lapse if there is a name change of the AIA or change in ownership.


CHIEF INSPECTOR



*Valid from: 27 May 2021
Expires: 26 May 2025
Certificate Number: CI MHI 0005*

15 APPENDIX D: SANAS CERTIFICATES



CERTIFICATE OF ACCREDITATION

In terms of section 22(2)(b) of the Accreditation for Conformity Assessment, Calibration and Good Laboratory Practice Act, 2006 (Act 19 of 2006), read with sections 23(1), (2) and (3) of the said Act, I hereby certify that:-

RISCOM (PTY) LTD
Co. Reg. No.: 2002/019697/07
JOHANNESBURG

Accreditation Number: **MHI0013**

is a South African National Accreditation System Accredited Inspection Body to undertake
TYPE A inspection provided that all SANAS conditions and requirements are complied with

This certificate is valid as per the scope as stated in the accompanying scope of accreditation,
Annexure "A", bearing the above accreditation number for

THE ASSESSMENT OF RISK ON MAJOR HAZARD INSTALLATIONS

The facility is accredited in accordance with the recognised International Standard

ISO/IEC 17020:2012 AND SANS 1461:2018

The accreditation demonstrates technical competency for a defined scope and the operation of a
management system

While this certificate remains valid, the Accredited Facility named above is authorised to use the
relevant SANAS accreditation symbol to issue facility reports and/or certificates

Mr M Phaloane
Acting Chief Executive Officer

Effective Date: 27 May 2021
Certificate Expires: 26 May 2025

This certificate does not on its own confer authority to act as an Approved Inspection Authority as contemplated in the Major
Hazard Installation Regulations. Approval to inspect within the regulatory domain is granted by the
Department of Employment and Labour.



ANNEXURE A
SCOPE OF ACCREDITATION

Accreditation Number: MHI0013

TYPE A

Permanent Address: Riscom (Pty) Ltd 33 Brighish Dr Northcliff Johannesburg 2195 Tel: (011) 431-2198 Fax: 086 624-9423 Mobile: 082 457-3258 E-mail: mike@riscom.co.za		Postal Address: P O Box 2541 Cresta Johannesburg 2195 Issue No.: 17 Date of issue: 25 May 2021 Expiry date: 26 May 2025
Nominated Representative: Mr MP Oberholzer	Quality Manager: Mr MP Oberholzer Technical Manager: Mr MP Oberholzer	Technical Signatory: Mr MP Oberholzer
Field of Inspection	Service Rendered	Codes and Regulations
Regulatory: The supply of services as an Inspection Authority for Major Hazard Risk Installation as defined in the Major Hazard Risk Installation Regulations, Government Notice No. R692 of 30 July 2001 Voluntary Supply of service as an inspection body for Hazard identification and analysis	Major Hazard Installation Risk Assessments for the following material categories: 1) Explosive chemicals 2) Gases: i) Flammable Gases ii) Non-flammable, non-toxic gases (asphyxiants) iii) Toxic gases 3) Flammable liquids 4) Flammable solids, substances liable to spontaneous combustion, substances that on contact with water release flammable gases 5) Oxidizing substances and organic peroxides 6) Toxic liquids and solids Hazard identification and analysis including HAZARD of and operability studies (HAZOP)	MHI regulation par. 5 (5) (b) i) Frequency/Probability Analysis ii) Consequence Modelling iii) Hazard Identification and Analysis iv) Emergency planning reviews Reference Manual Bevi Risk Assessments version 3.2 (2009) CPR 18E (1999), Guideline for quantitative risk assessment ("Purple Book"), TNO Apeldoorn. CPR 14E (1997). Methods for the Calculation of Physical Effects ("Yellow Book"), 3 rd Edition, TNO, Apeldoorn. CPR 16E (1992). Methods for the Determination of Possible Damage ("Green Book"), 1 st Edition, TNO, Apeldoorn. Lees FP (2001). Loss Prevention in the Process Industries: Hazard Identification, Assessment and Control, 2 nd Edition, Butterworths, London, UK. SANS 1461 SANS 31000 SANS 31010

Original date of accreditation: 27 May 2005

Page 1 of 1

ISSUED BY THE SOUTH AFRICAN NATIONAL ACCREDITATION SYSTEM

Accreditation Manager



forestry, fisheries & the environment

Department:
Forestry, Fisheries and the Environment
REPUBLIC OF SOUTH AFRICA

Private Bag X447, Pretoria, 0001, Environment House, 473 Steve Biko Road, Pretoria, 0002 Tel: +27 12 399 9000, Fax: +27 86 625 1042

SPECIALIST DECLARATION FORM – AUGUST 2023

Specialist Declaration form for assessments undertaken for application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

REPORT TITLE

Quantitative Risk Assessment of the Proposed CCGT at Kelvin Power Station, Kempton Park

Kindly note the following:

1. This form must always be used for assessment that are in support of applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting, where this Department is the Competent Authority.
2. This form is current as of August 2023. It is the responsibility of the Applicant / Environmental Assessment Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the Competent Authority. The latest available Departmental templates are available at <https://www.dffe.gov.za/documents/forms>.
3. An electronic copy of the signed declaration form must be appended to all Draft and Final Reports submitted to the department for consideration.
4. The specialist must be aware of and comply with 'the Procedures for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the act, when applying for environmental authorisation - GN 320/2020', where applicable.

1. SPECIALIST INFORMATION

Title of Specialist Assessment	Quantitative Risk Assessment
Specialist Company Name	Riscom
Specialist Name	Gillian Petzer
Specialist Identity Number	7512010074083
Specialist Qualifications:	BEng Chemical
Professional affiliation/registration:	Pr Eng
Physical address:	Click or tap here to enter text.
Postal address:	PO Box 2541
Postal address	Cresta 2118
Telephone	0114312198
Cell phone	0824573528
E-mail	mike@riscom.co.za

SPECIALIST DECLARATION FORM – AUGUST 2023

2. DECLARATION BY THE SPECIALIST

I, Gillian Petzer declare that –

- I act as the independent specialist in this application;
- I am aware of the procedures and requirements for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the National Environmental Management Act (NEMA), 1998, as amended, when applying for environmental authorisation which were promulgated in Government Notice No. 320 of 20 March 2020 (i.e. "the Protocols") and in Government Notice No. 1150 of 30 October 2020.
- I will perform the work relating to the application in an objective manner, even if this results in views and findings that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act, Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that reasonably has or may have the potential of influencing –
 - any decision to be taken with respect to the application by the competent authority; and
 - the objectivity of any report, plan or document to be prepared by myself for submission to the competent authority;
- All the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of Regulation 48 and is punishable in terms of section 24F of the NEMA Act.



Signature of the Specialist

Riscom

Name of Company:

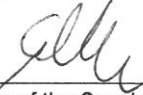
08 Aug 2024

Date

SPECIALIST DECLARATION FORM – AUGUST 2023

3. UNDERTAKING UNDER OATH/ AFFIRMATION

I, Gillian Petzer, swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct.



Signature of the Specialist

Riscom

Name of Company

8/8/2024

Date



Signature of the Commissioner of Oaths

08 Aug 2024

Date

